LINFOR3D User Manual

version 6.5.1

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Contents

1	Intro	oduction	7
2	Gett	ting started	8
3	3.1 3.2 3.3 3.4 3.5	Transfer equation for the continuum intensity Transfer equation for the line intensity Transfer equation for the line depression Contribution functions Grey test case	11 12 13 15
4	4.1 4.2 4.3	1	
5	Para 5.1	Program execution flags 2 5.1.1 run_flag 2 5.1.2 cv1_flag 2 5.1.3 cv2_flag 2 5.1.4 cv3_flag 2 5.1.5 plt_flag 2 5.1.6 maps_flag 2 5.1.7 cc3d_flag 2 5.1.8 nlte_flag 2 5.1.9 free_flag 2 General paths 3 5.2.1 abupath 3	
	5.3	5.2.3 opapath 2.4 gaspath 5.2.4 gaspath 2.5 eospath Model data 2.5 data 5.3.1 context 2.5 data 5.3.2 rhdpath 2.5 data 5.3.3 modelid 2.5 data 5.3.4 parfs 2.5 data 5.3.5 xbcpath 2.5 data 5.3.6 abuid 2.5 data 5.3.7 abuidx 2.5 data	26 27
	5.4	5.3.9 dalpha	28 29 29 29 29 30 30 30

5.4.6	Teff	80
5.4.7	grav	80
5.4.8	tsurffac	1
Model	data - reading of 'full' files (CO ⁵ BOLD only)	1
5.5.1	isnap_full_1	1
5.5.2	isnap_full_2	1
5.5.3	istep_full	1
⟨3D⟩ n	nean model	2
5.6.1	mavg	2
Extern	al 1D reference model	2
5.7.1	atmpath	32
5.7.2	atmfile	32
Line da	ata and radiative transfer	3
5.8.1	linfs	3
5.8.2	lutau1	3
5.8.3	lutau2	3
5.8.4	dlutau	3
5.8.5		3
5.8.6	lctau2	3
5.8.7		
5.8.8		
5.8.11		34
5.8.12		35
5.8.13		
5.8.15		
5.8.17		
5.8.18		
5.8.19	micro	6
5.8.20		6
5.8.21	xi_b	6
5.8.22	xi_d	6
5.8.23		37
5.8.24	intmode	37
5.8.25	intline	37
		37
Angle	quadrature schemes	8
5.9.1	•	88
5.9.2	nphi	88
5.9.3	•	88
5.9.4		8
5.9.5	1	9
		9
	1	9
		9
		0
		10
		1
	5.4.7 5.4.8 Model 5.5.1 5.5.2 5.5.3 ⟨3D⟩ m 5.6.1 Externa 5.7.1 5.7.2 Line da 5.8.1 5.8.2 5.8.3 5.8.4 5.8.5 5.8.6 5.8.7 5.8.8 5.8.10 5.8.11 5.8.12 5.8.13 5.8.14 5.8.15 5.8.16 5.8.17 5.8.18 5.8.19 5.8.20 5.8.21 5.8.22 5.8.23 5.8.24 5.8.25 5.8.26 Angle da 5.9.1 5.9.2 5.9.3 5.9.4 5.9.5 Curve- 5.10.1 5.10.2 5.10.3 5.10.4	5.4.7 grav 3.48 tsurffac 3.38 5.4.8 tsurffac 3.38 Model data - reading of 'full' files (CO⁵BOLD only) 3.5.5.1 isnap.full.2 5.5.2 isnap.full.2 3.5.5.3 istep.full (3D) mean model 3.3 5.6.1 mavg 3.5.7.1 atmpath 5.7.1 atmpath 3.5.7.2 atmfile 1.ine data and radiative transfer 3.5.8.1 lifts 5.8.2 lutaul 3.5.8.2 lutaul 5.8.3 blauau2 3.5.8.4 dlutau 5.8.4 dlutau 3.3 5.8.5 letaul 3.5.8.8 Hbrd 5.8.7 dletau 3.3 5.8.8.9 vsini 3.3 5.8.10 ximicx 3.3 5.8.11 ximicl 3.3 5.8.12 ximic3 3.3 5.8.13 ximacx 3.5 5.8.14 ximacl 3.3 5.8.15 ximac3 3.3 5.8.17 yfacy 3.3 5.8.18 vfacz 3.3 5.8.19 micro 3.3 5.8.19 micro 3.3 5.8.10 yia 3.3 5.8.11 ximcl 3.3 5.8.12 xi b 3.3 5.8.23 cleam 3.3

Line	Data F	le: line.dat
6.1	Parame	ers in Line Data File
	6.1.1	clam
	6.1.2	gfscale
6.2	Line D	ta Formats
	6.2.1	Continuum only
	6.2.2	Single line calculations, line data format '0'
	6.2.3	Single line calculations, line data format '1'
	6.2.4	Single line calculations, complete line data format '2'
	6.2.5	Single line calculations, complete line data format '3'
	6.2.6	Single line calculations, complete line data format '4'
	6.2.7	Single line calculations, complete line data format '5'
	6.2.7	· •
		Single line calculations, complete line data format '6'
	6.2.9	Single line calculations, complete line data format '7'
	6.2.10	Multiple Line Calculations
6.3		sion of line broadening parameters
	6.3.1	Quadratic Stark effect
	6.3.2	Van der Waals broadening
	6.3.3	ABO van der Waals broadening formalism
	6.3.4	Natural line broadening
04-	4 Cl	
-	out files	
7.1		
7.2		ore
7.3	Useful	JIO information
Outr	out file (· mustumos
-		t ructures D_1.uiosave
8.1		
	8.1.1	ABU
	8.1.2	ATOM
	8.1.3	CMD
	8.1.4	CONST
	8.1.5	INFO
	8.1.6	LINE
8.2	linfor_3	D_2.uiosave
	8.2.1	CONTF
	8.2.2	IMUPHI
	8.2.3	MAPS
	8.2.4	RESULT
8.3	linfor_3	D_3.uiosave
	8.3.1	CONTF3D
8.4	linfor_	X.uiosave
Plott	ing out	
	Plotting	the synthesis
9.1		contribution functions
9.1 9.2	Plotting	conditional functions
		the Curve-of-Growth
9.2		
9.2 9.3	Plotting	
9.2 9.3 0 Insta	Plotting	the Curve-of-Growth

12	ION	DIS																							79
	12.1	Atoms																							79
	12.2	Molecu	ıles																						80
		12.2.1	Soı	ne	def	init	ion	s.																	81
		12.2.2																							81
		12.2.3	•																						83
		12.2.4							_																84
		12.2.5			_																				85
		12.2.0					•5		•	 ·	•	 ·	 •	 •	•	•	 •	 •	 ·	•	 •	•	·	•	00
13	ionop	pa																							86
	13.1	temp.																							86
	13.2	pin .																							86
		alam.																							86
		pout .																							87
		densno																							87
		okappa																							87
		osigma																							87
		pgas .																							88
																									88
		namj.																							
)fracj																							88
		zeta .																							88
		2init.																							89
		3dm																							89
	13.14	ldalpha	a.						•	 •		 •	 •	 •			 •		 •		 •		•	•	89
	13.15	avm .																							89
	13.16	sehe .																							90
	13.17	abupa	th .																						90
	13.18	Rnami.																							90
	13.19	abui .																							90
	13.20)Examp	le .																						90
14	ionop																								92
		temp.							•	 •		 •	 •	 •			 •		 •		 •		•	•	92
	14.2	qin .																							92
	14.3	alam.																							92
	14.4	pe																							92
	14.5	pg																							93
	14.6	densno	с.																						93
	14.7	okappa	a .																						93
	14.8	osigma	a .																						93
	14.9	qflg.																							94
	14.10	namj.																							94
		fracj																							94
		zeta.																							94
		Binit.																							95
	14.14																								95
		dalpha																							95
	14.16	. •																							95
	14.17		 -h																						96
		Babupat																							96
		nami.																							96
	14.20	abui .																							96

6 LIST OF TABLES

14.2	1Example	97
List o	f Figures	
1	Analytical Curve-of-Growth	17
List o	f Tables	
1	List of all structures in common blocks 'linfordata'	20
2	List of additional IDL modules	20
3	List of all IDL modules	22
15	List of atoms	79
16	Small molecular network: 5 atoms, 8 molecules	80
17	Large molecular network:10 atoms, 14 molecules	81

1 Introduction

LINFOR3D is based on the old code LINFOR. Presently, there are two versions of the code: the one developed, tested and running in IDL, and the one developed, tested in IDL and running in Fortran 90. The latter has several advantages over the former, but both are still under development. Here is a short break down of the limitations of the code:

- **Geometry:** Both versions are limited to spectrum synthesis from **local hydrodynamical models** (solar-type convective atmospheres). In the future, it should be possible to compute the line formation in **global giant models**. However, this will mostly likely only occur in the Fortran 90 version, as this is the most actively developed version of the code.
- Efficiency: The IDL version of the code sees no *substantial* effort was yet taken to really improve the execution speed of this IDL/FORTRAN code. In fact there are still some parts in the code which are unnecessary for the current operation. Some effort has been applied to limit these unnecessary operations with additional run flags (see Sect. 5). However, further improvements to this are to be made.

The Fortran 90 version is newer, and as such has been developed to include some of the aformentioned version's limitations, including - but not limited to - removing the more unnecessary aspects of the code.

• **Parallel processing:** The newer versions of LINFOR3D (version 6.0.0 onwards) have been ported so that it runs on GDL as well as IDL. This means that parallel processing – as an embarassingly parallel job – is possible. See Sect. 10.2 for further information and updates. However, no effort has been made to add parallel processing in to the internal program flow of LINFOR3D.

The Fortran 90 version of the code has been developed with parallelization in mind. As such, the code is parallelized over several dimensions that are automatically sorted according to a priory decided by the code. The priority currently favours large sessions with many CPUs.

Like the code itself this user manual is under construction, too. Nevertheless, it will be of substantial help while installing LINFOR3D, creating new command and spectral line data files for LINFOR3D.

To get a brief overview of how to install and run LINFOR3D in its simplest form, you should read the section "Getting started" section (Sect. 2) first.

8 2 GETTING STARTED

2 Getting started

First make sure that you have all files which are listed in Tab. 3 and 2. These files should be put together in a directory which can be accessed under IDL (or GDL with versions 6.0.0 onwards).

The routines responsible for the most computationally expensive parts of LINFOR3D are called as external FORTRAN routines by linfor_3D_ionopa.pro and linfor_dort.pro. In order to properly run LINFOR3D, the Linux path variable \$IDL_SO should be defined. After unpacking LINFOR3D, create a new sub-directory within the directory tree called bin, then define IDL_SO:

```
> export IDL_SO=<LINFOR_DIRECTORY>/bin/
```

This needs to be added to your Linux login script to be consistently defined by your Linux OS. Next you need to compile the FORTRAN libraries dort_idl.so and ionopa2_idl.so. By default, these libraries use the Intel[©] FORTRAN, IFORT, compilers. This is done by running the Makefile script in xmono:

```
> make -f Makefile
```

Other methods of compilation are available, but Makefile needs to be appropriately edited. If \$IDL_SO is properly defined, the two libraries should compile and be moved to the bin sub-directory.

Now two files have to be edited and provided in order to run LINFOR3D:

• linfor_setcmd.pro:

This file, which is an IDL script, defines the data structure cmd. This structure contains all necessary information (except for spectral line data) like, e.g., paths and names of model file(s). See Sect. 5 for more details.

• line.dat:

This file contains all data for spectral line such as, e.g., oscillator strength and broadening parameters. The usual file name is line.dat but it might be given another name which then has be to entered in linfor_setcmd.pro. See Sect. 6 for more details.

Finally, all versions of LINFOR3D require the "Universal Input Output" (UIO) routine library (written by B. Freytag) for I/O related to CO⁵BOLD files, and version 6.0.0 onwards requires them for <u>ALL</u> I/O done during its execution. This must be defined in the \$IDL_PATH. After doing so, you can run LINFOR3D by starting IDL or GDL (see Sect. 10) and type:

```
IDL> .r linfor_3D.pro
```

Several output files are created. It is possible to load these files in IDL or GDL. See Sect. 7 for more details.

Normally, one uses a bespoke linfor_setcmd.pro file in a directory of their choosing. If this is the case then one must start IDL or GDL in the proper sub-directory and then type the following:

```
IDL> common linfordata, info, cmd, const, atom, abu, line, gas, eos, result
IDL> .com bespoke_linfor_setcmd.pro
% Compiled module: LINFOR_SETCMD.
IDL> .r linfor_3D.pro
```

One of the most efficient ways to run LINFOR3D is to create an IDL/GDL wrapper around one's bespoke setcmd program, as the following example depicts:

```
common linfordata, info, cmd, const, atom, abu, line, gas, eos, result
.compile bespoke_linfor_setcmd.pro
.run linfor_3D.pro
if keyword_set(cmd.cc3d_flag) then $
uio_save, filename = 'output.uiosave', /verbose, $
info, cmd, const, atom, abu, line, result, maps, imuphi, contf, contf3d $
else $
uio_save, filename = 'output.uiosave', /verbose, $
info, cmd, const, atom, abu, line, result, maps, imuphi, contf
exit
```

This runs the bespoke LINFOR3D script and saves the entire output as a tailored save file, as well as the default uiosave files usually output by LINFOR3D that splits the contents of the structures mostly defined in linfordata.

Note that LINFOR3D stores the flow field in temporary cache files which are automatically restored if the same calculation is repeated! This feature has been retired in LINFOR3D versions 6.0.0 onwards.

Important changes that could affect your output have been made in LINFOR3D version 6.2.6 onwards. Please read Sect. 5.4 carefully.

A brief description of the changes made for all LINFOR3D releases (up to the version you are running) is given in readme_<version> given in the top directory of your LINFOR3D installation.

3 Basic Equations of Radiative Transfer

3.1 Transfer equation for the continuum intensity

$$\frac{\mathrm{d}I_{\lambda}^{c}}{\mathrm{d}s} = -\kappa_{\lambda}^{c}I_{\lambda}^{c} + \kappa_{\lambda}^{c}S_{\lambda}^{c} \tag{1}$$

together with the definition of the optical depth along the ray

$$d\tau_{\lambda}^{c} = -\kappa_{\lambda}^{c} ds, \qquad (2)$$

reads

$$\frac{\mathrm{d}\,I_{\lambda}^{c}}{\mathrm{d}\,\tau_{\lambda}^{c}} = I_{\lambda}^{c} - S_{\lambda}^{c}.\tag{3}$$

The solution of Eq. (3) is

$$I_{\lambda}^{c}(\tau_{\lambda}^{c}) = \int_{\tau_{\lambda}^{c}}^{\tau_{\lambda}^{b}} S_{\lambda}^{c}(\tau') \exp\{-(\tau' - \tau_{\lambda}^{c})\} d\tau' + I_{\lambda}^{c}(\tau_{\lambda}^{b}) \exp\{-(\tau_{\lambda}^{b} - \tau_{\lambda}^{c})\}$$

$$(4)$$

where τ_{λ}^{b} is the continuum optical depth at the lower boundary. The **emergent** continuum intensity is:

$$I_{\lambda}^{c}(\tau_{\lambda}^{c}=0) = \int_{0}^{\tau_{\lambda}^{b}} S_{\lambda}^{c}(\tau') \exp\{-\tau'\} d\tau' + I_{\lambda}^{c}(\tau_{\lambda}^{b}) \exp\{-\tau_{\lambda}^{b}\}.$$
 (5)

Defining

$$u_{\lambda}^{c} = I_{\lambda}^{c} - S_{\lambda}^{c} \tag{6}$$

we have the transport equation

$$\frac{\mathrm{d}\,u_{\lambda}^{c}}{\mathrm{d}\,\tau_{\lambda}^{c}} = u_{\lambda}^{c} - \frac{\mathrm{d}\,S_{\lambda}^{c}}{\mathrm{d}\,\tau_{\lambda}^{c}}\,.\tag{7}$$

The solution for u_{λ}^{c} is found by replacing S_{λ}^{c} by $dS_{\lambda}^{c}/d\tau_{\lambda}^{c}$ in Eq.(4):

$$u_{\lambda}^{c}(\tau_{\lambda}^{c}) = \int_{\tau_{\lambda}^{c}}^{\tau_{\lambda}^{b}} \frac{\mathrm{d}S_{\lambda}^{c}(\tau')}{\mathrm{d}\tau_{\lambda}^{c}} \exp\{-(\tau' - \tau_{\lambda}^{c})\} \,\mathrm{d}\tau' + u_{\lambda}^{c}(\tau_{\lambda}^{b}) \exp\{-(\tau_{\lambda}^{b} - \tau_{\lambda}^{c})\}$$
(8)

The emergent intensity can also be obtained from Eq.(8):

$$I_{\lambda}^{c}(\tau_{\lambda}^{c}=0) = S_{\lambda}^{c}(\tau_{\lambda}^{c}=0) + \int_{0}^{\tau_{\lambda}^{b}} \frac{\mathrm{d}S_{\lambda}^{c}(\tau')}{\mathrm{d}\tau_{\lambda}^{c}} \exp\{-\tau'\} \,\mathrm{d}\tau' + u_{\lambda}^{c}(\tau_{\lambda}^{b}) \exp\{-\tau_{\lambda}^{b}\}. \tag{9}$$

Now we define a fixed central wavelength, λ_0 , with the corresponding **fixed (universal) optical depth** scale τ_0 , which is equidistant in $\log \tau_0$ and may used alternatively for all integrations. On this optical depth scale, Eq.(4) becomes

$$I_{\lambda}^{c}(\tau_{0}) = \int_{\tau_{0}}^{\tau_{0}^{b}} \frac{\kappa_{\lambda}^{c}}{\kappa_{0}^{c}} S_{\lambda}^{c}(\tau_{0}^{\prime}) \exp\{-\left(\tau_{\lambda}^{c}(\tau_{0}^{\prime}) - \tau_{\lambda}^{c}(\tau_{0})\right)\} d\tau_{0}^{\prime} + I_{\lambda}^{c}(\tau_{0}^{b}) \exp\{-\left(\tau_{\lambda}^{c}(\tau_{0}^{b}) - \tau_{\lambda}^{c}(\tau_{0})\right)\},$$
 (10)

giving the continuum intensity at wavelength λ as a function of optical depth τ_0 . Note the factor $\kappa_{\lambda}^c/\kappa_0^c$ under the integral. The intensity at the lower boundary, $I_{\lambda}^c(\tau_0^b)$, can be computed from the diffusion approximation,

$$I_{\lambda}^{c}(\tau_{0}^{b}) = S_{\lambda}^{c}(\tau_{0}^{b}) + \frac{\kappa_{0}^{c}}{\kappa_{\lambda}^{c}} \frac{\mathrm{d} S_{\lambda}^{c}}{\mathrm{d} \tau_{0}}(\tau_{0}^{b}), \tag{11}$$

but the boundary term may also be neglected, at least for the emergent intensity, because the exponential factor is usually very small. For the **emergent** intensity we have from Eq.(5):

$$I_{\lambda}^{c}(\tau_{0}=0) = \int_{0}^{\tau_{0}^{b}} \frac{\kappa_{\lambda}^{c}}{\kappa_{0}^{c}} S_{\lambda}^{c}(\tau_{0}^{\prime}) \exp\{-\tau_{\lambda}^{c}(\tau_{0}^{\prime})\} d\tau_{0}^{\prime} + I_{\lambda}^{c}(\tau_{0}^{b}) \exp\{-\tau_{\lambda}^{c}(\tau_{0}^{b})\}.$$
 (12)

Similarly, Eq.(8) becomes

$$u_{\lambda}^{c}(\tau_{0}) = \int_{\tau_{0}}^{\tau_{0}^{b}} \frac{\mathrm{d} S_{\lambda}^{c}}{\mathrm{d} \tau_{0}}(\tau_{0}^{c}) \exp\{-\tau_{\lambda}^{c}(\tau_{0}^{c}) - \tau_{\lambda}^{c}(\tau_{0})\} \,\mathrm{d} \tau_{0}^{c} + u_{\lambda}^{c}(\tau_{0}^{b}) \exp\{-\tau_{\lambda}^{c}(\tau_{0}^{b}) - \tau_{\lambda}^{c}(\tau_{0})\}. \tag{13}$$

Note the absence of the factor $\kappa_{\lambda}^{c}/\kappa_{0}^{c}$ under the integral in this case. $u_{\lambda}^{c}(\tau_{0}^{b})$ is obtained from the diffusion approximation,

$$u_{\lambda}^{c}(\tau_{0}^{b}) = \frac{\kappa_{0}^{c}}{\kappa_{\lambda}^{c}} \frac{\mathrm{d} S_{\lambda}^{c}}{\mathrm{d} \tau_{0}}(\tau_{0}^{b}). \tag{14}$$

The emergent intensity can be computed from Eq.(13) as:

$$I_{\lambda}^{c}(\tau_{0}=0) = S_{\lambda}^{c}(\tau_{0}=0) + \int_{0}^{\tau_{0}^{b}} \frac{dS_{\lambda}^{c}}{d\tau_{0}}(\tau_{0}^{\prime}) \exp\{-\tau_{\lambda}^{c}(\tau_{0}^{\prime})\} d\tau_{0}^{\prime} + u_{\lambda}^{c}(\tau_{0}^{b}) \exp\{-\tau_{\lambda}^{c}(\tau_{0}^{b})\}.$$
 (15)

In the latest version of Linfor3D, the continuum intensity is calculated from Eqs.(8) and (9), at 3 different wavelengths: $\lambda_0 - \Delta \lambda$, λ_0 , and $\lambda_0 + \Delta \lambda$, where $\Delta \lambda$ is specified by the parameter dclam. We ensure that the derivative d $S_0^2/d\tau_0$ fulfills the condition

$$\int_{\tau_1}^{\tau_2} \frac{\mathrm{d} S_{\lambda}^c}{\mathrm{d} \tau_{\lambda}} (\tau_{\lambda}') \, \mathrm{d} \tau_{\lambda}' = S_{\lambda}^c(\tau_2) - S_{\lambda}^c(\tau_1) \,. \tag{16}$$

The reason for using Eqs.(8) and (9) instead of Eq.(5) is that the quantity $u_{\lambda}^{c}(\tau)$ is needed to compute the line depression source function (see Sect. 3.3). We have checked that the usual transfer equation, Eq.(5), gives numerically very closely the same results for the emergent continuum intensity as Eq.(9).

3.2 Transfer equation for the line intensity

In the presence of lines, the transfer equation at wavelength λ reads

$$\frac{\mathrm{d}I_{\lambda}^{\ell}}{\mathrm{d}s} = -\left(\kappa_{\lambda}^{c} + \sum_{\ell} \kappa_{\lambda}^{\ell}\right) I_{\lambda}^{\ell} + \kappa_{\lambda}^{c} S_{\lambda}^{c} + \sum_{\ell} \kappa_{\lambda}^{\ell} S_{\lambda}^{\ell}. \tag{17}$$

The line source functions S_{λ}^{ℓ} may be different from the LTE continuum source function S_{λ}^{c} . With the definition of the total optical depth

$$d\tau_{\lambda} = -\left(\kappa_{\lambda}^{c} + \sum_{\ell} \kappa_{\lambda}^{\ell}\right) ds \equiv d\tau_{\lambda}^{c} + d\tau_{\lambda}^{\ell}, \qquad (18)$$

and the total source function

$$S_{\lambda} = \frac{\kappa_{\lambda}^{c} S_{\lambda}^{c}}{\kappa_{\lambda}^{c} + \sum_{\ell} \kappa_{\lambda}^{\ell}} + \frac{\sum_{\ell} \kappa_{\lambda}^{\ell} S_{\lambda}^{\ell}}{\kappa_{\lambda}^{c} + \sum_{\ell} \kappa_{\lambda}^{\ell}} = \frac{S_{\lambda}^{c} + \eta \overline{S_{\lambda}^{\ell}}}{1 + \eta} = \frac{1 + \beta}{1 + \eta} S_{\lambda}^{c}, \tag{19}$$

where

$$\overline{S_{\lambda}^{\ell}} = \frac{\sum_{\ell} \kappa_{\lambda}^{\ell} S_{\lambda}^{\ell}}{\sum_{\ell} \kappa_{\lambda}^{\ell}}, \quad \eta = \frac{\sum_{\ell} \kappa_{\lambda}^{\ell}}{\kappa_{\lambda}^{c}}, \quad \beta = \frac{\sum_{\ell} \kappa_{\lambda}^{\ell} S_{\lambda}^{\ell}}{\kappa_{\lambda}^{c} S_{\lambda}^{c}}, \quad (20)$$

we can write

$$\frac{\mathrm{d}I_{\lambda}^{\ell}}{\mathrm{d}\tau_{\lambda}} = I_{\lambda}^{\ell} - S_{\lambda}. \tag{21}$$

In LTE, $S_{\lambda} = S_{\lambda}^{c}$. The solution of Eq.(21) is

$$I_{\lambda}^{\ell}(\tau_{\lambda} = 0) = \int_{0}^{\tau_{\lambda}^{\ell}} S_{\lambda}(\tau_{\lambda}^{\prime}) \exp\{-\tau_{\lambda}^{\prime}\} d\tau_{\lambda}^{\prime} + I_{\lambda}^{\ell}(\tau_{\lambda}^{b}) \exp\{-\tau_{\lambda}^{b}\}.$$
 (22)

In analogy to Eq.(12), we can also obtain the emergent line intensity by integration on the universal optical depth scale τ_0 :

$$I_{\lambda}^{\ell}(\tau_{0}=0) = \int_{0}^{\tau_{0}^{b}} \frac{\kappa_{\lambda}^{c}}{\kappa_{0}^{c}} (1+\eta) S_{\lambda}(\tau_{0}^{\prime}) \exp\{-\tau_{\lambda}(\tau_{0}^{\prime})\} d\tau_{0}^{\prime} + I_{\lambda}^{\ell}(\tau_{0}^{b}) \exp\{-\tau_{\lambda}(\tau_{0}^{b})\},$$
 (23)

or, substituting S_{λ} from Eq.(19),

$$I_{\lambda}^{\ell}(\tau_{0}=0) = \int_{0}^{\tau_{0}^{b}} \frac{\kappa_{\lambda}^{c}}{\kappa_{0}^{c}} (1+\beta) S_{\lambda}^{c}(\tau_{0}^{\prime}) \exp\{-\tau_{\lambda}(\tau_{0}^{\prime})\} d\tau_{0}^{\prime} + I_{\lambda}^{\ell}(\tau_{0}^{b}) \exp\{-\tau_{\lambda}(\tau_{0}^{b})\}.$$
 (24)

Integration on the $\log \tau_0$ scale $(z_0 \equiv \log \tau_0)$ gives:

$$I_{\lambda}^{\ell}(z_{0}^{a}) = \int_{z_{0}^{a}}^{z_{0}^{b}} \ln(10) \, \tau_{0}(z_{0}^{\prime}) \, \frac{\kappa_{\lambda}^{c}}{\kappa_{0}^{c}} (1 + \beta) \, S_{\lambda}^{c}(z_{0}^{\prime}) \, \exp\{-\tau_{\lambda}(z_{0}^{\prime})\} \, \mathrm{d} \, z_{0}^{\prime} + I_{\lambda}^{\ell}(z_{0}^{b}) \, \exp\{-\tau_{\lambda}(z_{0}^{b})\} \,, \tag{25}$$

where z_0^a is the minimum log optical depth. Alternatively, in analogy to Eq.(9) we obtain:

$$I_{\lambda}^{\ell}(\tau_{\lambda} = 0) = S_{\lambda}(\tau_{\lambda} = 0) + \int_{0}^{\tau_{\lambda}^{b}} \frac{\mathrm{d}S_{\lambda}}{\mathrm{d}\tau_{\lambda}}(\tau_{\lambda}^{\prime}) \exp\{-\tau_{\lambda}^{\prime}\} \,\mathrm{d}\tau_{\lambda}^{\prime} + u_{\lambda}^{\ell}(\tau_{\lambda}^{b}) \exp\{-\tau_{\lambda}^{b}\}, \tag{26}$$

where we have defined

$$u_{\lambda}^{\ell} = I_{\lambda}^{\ell} - S_{\lambda}, \tag{27}$$

which in the diffusion approximation may be written as

$$u_{\lambda}^{\ell}(\tau_{\lambda}^{b}) = \frac{\mathrm{d}S_{\lambda}}{\mathrm{d}\tau_{\lambda}}(\tau_{\lambda}^{b}) \quad \text{or} \quad u_{\lambda}^{\ell}(\tau_{0}^{b}) = \frac{\kappa_{0}^{c}/\kappa_{\lambda}^{c}}{1+\eta} \frac{\mathrm{d}S_{\lambda}}{\mathrm{d}\tau_{0}}(\tau_{0}^{b}). \tag{28}$$

On the universal optical depth scale τ_0 we obtain from Eq.(26:

$$I_{\lambda}^{\ell}(\tau_{0}=0) = S_{\lambda}(\tau_{0}=0) + \int_{0}^{\tau_{0}^{b}} \frac{\mathrm{d}S_{\lambda}}{\mathrm{d}\tau_{0}}(\tau_{0}^{\prime}) \exp\{-\tau_{\lambda}(\tau_{0}^{\prime})\} \,\mathrm{d}\tau_{0}^{\prime} + u_{\lambda}^{\ell}(\tau_{0}^{b}) \exp\{-\tau_{\lambda}(\tau_{0}^{b})\}, \tag{29}$$

In LTE, where $S_{\lambda} = S_{\lambda}^{c}$, the integral in Eq.(29) differs from the integral in Eq.(15) only by the exponential factor which involves the total optical depth τ_{λ} instead of the continuum optical depth τ_{λ}^{c} . The absolute line depression is then calculated as

$$D_{\lambda} = I_{\lambda}^{c}(\tau = 0) - I_{\lambda}^{\ell}(\tau = 0). \tag{30}$$

In the current version of Linfor3D, Eq.(25) is used if the parameter intline is set to -1, and Eq.(26) is used if intline is set to -2.

3.3 Transfer equation for the line depression

We may analyse the transfer equation for the absolute line depression defined in Eq.(30):

$$\frac{\mathrm{d}D_{\lambda}}{\mathrm{d}s} = \frac{\mathrm{d}I_{\lambda}^{c}}{\mathrm{d}s} - \frac{\mathrm{d}I_{\lambda}^{\ell}}{\mathrm{d}s} = -\kappa_{\lambda}^{c}I_{\lambda}^{c} + \left(\kappa_{\lambda}^{c} + \sum_{\ell} \kappa_{\lambda}^{\ell}\right)I_{\lambda}^{\ell} - \sum_{\ell} \kappa_{\lambda}^{\ell}S_{\lambda}^{\ell}$$
(31)

or

$$\frac{\mathrm{d}D_{\lambda}}{\mathrm{d}s} = -\left(\kappa_{\lambda}^{c} + \sum_{\ell} \kappa_{\lambda}^{\ell}\right) D_{\lambda} + \left(I_{\lambda}^{c} \sum_{\ell} \kappa_{\lambda}^{\ell} - \sum_{\ell} \kappa_{\lambda}^{\ell} S_{\lambda}^{\ell}\right)$$
(32)

or

$$\frac{\mathrm{d}D_{\lambda}}{\mathrm{d}\tau_{\lambda}} = D_{\lambda} - S_{\lambda}^{D},\tag{33}$$

where the line depression source function is

$$S_{\lambda}^{D} = \frac{\eta}{1+\eta} \left(I_{\lambda}^{c} - \overline{S_{\lambda}^{\ell}} \right) = \frac{\eta}{1+\eta} \left((I_{\lambda}^{c} - S_{\lambda}^{c}) + (S_{\lambda}^{c} - \overline{S_{\lambda}^{\ell}}) \right). \tag{34}$$

In LTE, $\overline{S_{\lambda}^{\ell}} = S_{\lambda}^{c}$, and

$$S_{\lambda}^{D} = \frac{\eta}{1+\eta} \left(I_{\lambda}^{c} - S_{\lambda}^{c} \right). \tag{35}$$

The solution of Eq.(33) is

$$D_{\lambda}(\tau_{\lambda} = 0) = \int_{0}^{\tau_{\lambda}^{b}} S_{\lambda}^{D}(\tau_{\lambda}') \exp\{-\tau_{\lambda}'\} d\tau_{\lambda}', \tag{36}$$

neglecting the boundary term. Integration on the fixed τ_0 scale:

$$D_{\lambda}(\tau_0 = 0) = \int_0^{\tau_0^b} \frac{\kappa_{\lambda}^c}{\kappa_0^c} (1 + \eta) S_{\lambda}^D(\tau_0') \exp\{-\tau_{\lambda}(\tau_0')\} d\tau_0'.$$
 (37)

Substituting S_{λ}^{D} from Eq.(34) gives

$$D_{\lambda}(\tau_0 = 0) = \int_0^{\tau_0^b} \frac{\kappa_{\lambda}^c}{\kappa_0^c} \eta \left(I_{\lambda}^c - \overline{S_{\lambda}^{\ell}} \right) \exp\{-\tau_{\lambda}(\tau_0')\} d\tau_0', \tag{38}$$

where κ_{λ}^c , κ_0^c , η , I_{λ}^c , $\overline{S_{\lambda}^{\ell}}$, and τ_{λ} are defined as a function of τ_0 . We can also write

$$D_{\lambda}(\tau_{0} = 0) = \int_{0}^{\tau_{0}^{b}} \frac{\kappa_{\lambda}^{c}}{\kappa_{0}^{c}} \eta \left(u_{\lambda}^{c} + (S_{\lambda}^{c} - \overline{S_{\lambda}^{\ell}}) \right) \exp\{-\tau_{\lambda}(\tau_{0}^{\prime})\} d\tau_{0}^{\prime},$$
 (39)

where

$$\frac{\eta}{1+\eta} \left(S_{\lambda}^{c} - \overline{S_{\lambda}^{\ell}} \right) = S_{\lambda}^{c} \frac{(\eta - \beta)}{1+\eta} \tag{40}$$

is the NLTE correction to the line depression source function. Integration on the $\log \tau_0$ scale ($z_0 \equiv \log \tau_0$) gives:

$$D_{\lambda}(z_0^a) = \int_{z_0^a}^{z_0^b} \ln(10) \, \tau_0(z_0') \, \frac{\kappa_{\lambda}^c}{\kappa_0^c} \, \eta \, \left(u_{\lambda}^c + (S_{\lambda}^c - \overline{S_{\lambda}^\ell}) \right) \exp\{-\tau_{\lambda}(z_0')\} \, \mathrm{d} \, z_0' \,. \tag{41}$$

In the current version of Linfor3D, Eq.(41) is used to compute the line depression if the parameter intline is set to 1, while Eq.(36) is used if intline = 2.

3.4 Contribution functions

The Continuum Intensity Contribution Function for a ray with inclination angle $\mu = \cos \theta$, azimuthal angle ϕ , and wavelength λ is simply the horizontal average of the integrand of Eq.(12)

$$C_I^c(\tau_0, \mu, \phi, \lambda) = \frac{1}{\mu} \left\langle \frac{\kappa_{\lambda}^c}{\kappa_0^c} S_{\lambda}^c(\tau_0/\mu) \exp\{-\tau_{\lambda}^c(\tau_0/\mu)\} \right\rangle_{x,y}, \tag{42}$$

such that

$$I_{\lambda}^{c}(\tau_{0} = 0, \mu, \phi, \lambda) = \int_{0}^{\tau_{0}^{b}} C_{I}^{c}(\tau_{0}^{\prime}, \mu, \phi, \lambda) \, d\tau_{0}^{\prime} = \int_{0}^{z_{0}^{b}} \ln(10) \, \tau_{0}(z_{0}^{\prime}) \, C_{I}^{c}(\tau_{0}(z_{0}^{\prime}), \mu, \phi, \lambda) \, dz_{0}^{\prime}. \tag{43}$$

Note that now (τ_0/μ) is the optical depth along the line-of-sight, and τ_0 is the corresponding vertical optical depth (a formal quantity in the presence of horizontal inhomogeneities).

The Continuum Flux Contribution Function at wavelength λ is consequently

$$C_F^c(\tau_0, \lambda) = \int_0^{2\pi} \int_0^1 \mu' \, C_I^c(\tau_0, \mu', \phi', \lambda) \, \mathrm{d}\mu' \, \mathrm{d}\phi' \,, \tag{44}$$

such that

$$F_{\lambda}^{c}(\tau_{0}=0,\lambda) = \int_{0}^{\tau_{0}^{b}} C_{F}^{c}(\tau_{0}',\lambda) \,\mathrm{d}\,\tau_{0}' = \int_{0}^{z_{0}^{b}} \ln(10)\,\tau_{0}(z_{0}') \,C_{F}^{c}(\tau_{0}(z_{0}'),\lambda) \,\mathrm{d}\,z_{0}'. \tag{45}$$

Note that the horizontal averaging in Eq.(42) works only because the transfer equation is integrated on the fixed universal optical depth scale, τ_0 . The contribution functions $C_I^c(\tau_0, \mu_0, \phi_0, \lambda_0)$ and $C_F^c(\tau_0, \lambda_0)$ are saved in contf.cfc3i and contf.cfc3f, respectively. Corresponding contribution functions are also computed for the $\langle 3D \rangle$ model and saved in contf.cfc1i and contf.cfc1f, respectively, and for the external 1D reference atmosphere (contf.cfcxi and contf.cfcxf).

Similarly, we can also write down the <u>Line Intensity Contribution Function</u> as the horizontal average of the integrand of Eq.(24):

$$C_I^{\ell}(\tau_0, \mu, \phi, \lambda) = \frac{1}{\mu} \left\langle \frac{\kappa_{\lambda}^{c}}{\kappa_0^{c}} (1 + \beta) S_{\lambda}^{c}(\tau_0/\mu) \exp\{-\tau_{\lambda}(\tau_0/\mu)\} \right\rangle_{x,\mu}, \tag{46}$$

such that the intensity at a given wavelength in the line profile is

$$I_{\lambda}^{\ell}(\tau_{0}=0,\mu,\phi,\lambda) = \int_{0}^{\tau_{0}^{b}} C_{I}^{\ell}(\tau_{0}',\mu,\phi,\lambda) \,\mathrm{d}\,\tau_{0}' = \int_{0}^{z_{0}^{b}} \ln(10)\,\tau_{0}(z_{0}') \,C_{I}^{\ell}(\tau_{0}(z_{0}'),\mu,\phi,\lambda) \,\mathrm{d}\,z_{0}' \,. \tag{47}$$

The Line Flux Contribution Function at wavelength λ is

$$C_F^{\ell}(\tau_0, \lambda) = \int_0^{2\pi} \int_0^1 \mu' \, C_I^{\ell}(\tau_0, \mu', \phi', \lambda) \, \mathrm{d}\mu' \, \mathrm{d}\phi' \,, \tag{48}$$

such that

$$F_{\lambda}^{\ell}(\tau_{0}=0,\lambda) = \int_{0}^{\tau_{0}^{b}} C_{F}^{\ell}(\tau_{0}',\lambda) \,\mathrm{d}\,\tau_{0}' = \int_{0}^{z_{0}^{b}} \ln(10)\,\tau_{0}(z_{0}') \,C_{F}^{\ell}(\tau_{0}(z_{0}'),\lambda) \,\mathrm{d}\,z_{0}' \,. \tag{49}$$

 $C_I^{\ell}(\tau_0, \mu_0, \phi_0, \lambda_0)$ and $C_F^{\ell}(\tau_0, \lambda_0)$ are stored in contf.cfl3i and contf.cfl3f, respectively, and similarly for the 1D atmospheres in contf.cfl1i, contf.cfl1f, contf.cflxi, and contf.cflxf.

Formally, a Line Depression Contribution Function could be defined as

$$\tilde{C}_{I}^{D} = C_{I}^{c} - C_{I}^{\ell} = \frac{1}{\mu} \left\langle \frac{\kappa_{\lambda}^{c}}{\kappa_{0}^{c}} S_{\lambda}^{c}(\tau_{0}/\mu) \exp\{-\tau_{\lambda}^{c}(\tau_{0}/\mu)\} \left(1 - (1 + \beta) \exp\{-\tau_{\lambda}^{\ell}(\tau_{0}/\mu)\}\right) \right\rangle_{x,y},$$
 (50)

such that the absolute line depression at any wavelength in the line profile is

$$D_{I}(\tau_{0} = 0, \mu, \phi, \lambda) = \int_{0}^{\tau_{0}^{b}} \tilde{C}_{I}^{D}(\tau_{0}', \mu, \phi, \lambda) d\tau_{0}' = \int_{0}^{z_{0}^{b}} \ln(10) \tau_{0}(z_{0}') \tilde{C}_{I}^{D}(\tau_{0}(z_{0}'), \mu, \phi, \lambda) dz_{0}'.$$
 (51)

Note however, that \tilde{C}_I^D does not have the desired physical meaning, because the factor $(1-(1+\beta)\exp\{-\tau_{\lambda}^{\ell}\})$ (i) becomes negative when τ_{λ}^{ℓ} is small $(\tau_{\lambda}^{\ell}$ is the optical depth due to the line opacity only), and (ii) it is non-zero also in layers where the line opacity vanishes. For this reason, \tilde{C}_I^D is not considered useful and hence is not computed in the current version of LINFOR3D.

A much better way to define the <u>Line Depression Contribution Function</u> is to consider Eq.(39) and to define it as

$$C_I^D(\tau_0, \mu, \phi, \lambda) = \frac{1}{\mu} \left\langle \frac{\kappa_{\lambda}^c}{\kappa_0^c} \left(\eta \, u_{\lambda}^c(\tau_0/\mu) + (\eta - \beta) \, S_{\lambda}^c(\tau_0/\mu) \right) \exp\{-\tau_{\lambda}(\tau_0/\mu)\} \right\rangle_{x,y}. \tag{52}$$

Note that this contribution function vanisches whereever the line opacity (η, β) is zero. For the flux spectrum we define, as before,

$$C_F^D(\tau_0, \lambda) = \int_0^{2\pi} \int_0^1 \mu' \, C_I^D(\tau_0, \mu', \phi', \lambda) \, \mathrm{d}\mu' \, \mathrm{d}\phi' \,. \tag{53}$$

3.5 Grey test case

Then the absolute line depression at any wavelength in the line profile is

$$D_{I}(\tau_{0} = 0, \mu, \phi, \lambda) = \int_{0}^{\tau_{0}^{b}} C_{I}^{D}(\tau'_{0}, \mu, \phi, \lambda) d\tau'_{0} = \int_{0}^{z_{0}^{b}} \ln(10) \tau_{0}(z'_{0}) C_{I}^{D}(\tau_{0}(z'_{0}), \mu, \phi, \lambda) dz'_{0},$$
 (54)

and

$$D_F(\tau_0 = 0, \lambda) = \int_0^{\tau_0^b} C_F^D(\tau_0', \lambda) \, \mathrm{d}\, \tau_0' = \int_0^{z_0^b} \ln(10) \, \tau_0(z_0') \, C_F^D(\tau_0(z_0'), \lambda) \, \mathrm{d}\, z_0', \tag{55}$$

for the intensity and flux spectrum, respectively.

The Equivalent Width Contribution Function is computed as

$$C_I^W(\tau_0, \mu, \phi) = \int_{\lambda} C_I^D(\tau_0, \mu, \phi, \lambda') d\lambda', \qquad (56)$$

and

$$W_{I}(\mu,\phi) = \frac{1}{\langle I_{\lambda}^{c}(\mu,\phi,\lambda)\rangle} \int_{0}^{\tau_{0}^{b}} C_{I}^{W}(\tau_{0}',\mu,\phi) d\tau_{0}'$$

$$= \frac{1}{\langle I_{\lambda}^{c}(\mu,\phi,\lambda)\rangle} \int_{0}^{z_{0}^{b}} \ln(10) \tau_{0}(z_{0}') C_{I}^{W}(\tau_{0}(z_{0}'),\mu,\phi) dz_{0}',$$
(57)

where

$$\langle I_{\lambda}^{c}(\mu,\phi,\lambda)\rangle = \frac{\int_{\lambda} D_{I}(\mu,\phi,\lambda') \,\mathrm{d}\,\lambda'}{\int_{\lambda} D_{I}(\mu,\phi,\lambda')/I_{\lambda}^{c}(\mu,\phi,\lambda') \,\mathrm{d}\,\lambda'}.$$
 (58)

For the flux spectrum we have

$$C_F^W(\tau_0) = \int_{\lambda} C_F^D(\tau_0, \lambda') \mathrm{d}\lambda', \qquad (59)$$

and

$$W_{F} = \frac{1}{\langle F_{\lambda}^{c}(\lambda) \rangle} \int_{0}^{\tau_{0}^{b}} C_{F}^{W}(\tau_{0}') d\tau_{0}'$$

$$= \frac{1}{\langle F_{\lambda}^{c}(\lambda) \rangle} \int_{0}^{z_{0}^{b}} \ln(10) \tau_{0}(z_{0}') C_{F}^{W}(\tau_{0}(z_{0}')) dz_{0}',$$
(60)

with

$$\langle F_{\lambda}^{c}(\lambda) \rangle = \frac{\int_{\lambda} D_{F}(\lambda') \, \mathrm{d} \, \lambda'}{\int_{\lambda} D_{F}(\lambda') / F_{\lambda}^{c}(\lambda') \, \mathrm{d} \, \lambda'} \,. \tag{61}$$

Irrespective of the parameter intline, the structures contf.cfd3i and contf.cfd3f hold the contribution functions $C_I^D(\tau_0,\mu 0,\phi_0,\lambda 0)$ and $C_F^D(\tau_0,\lambda 0)$, while $C_I^W(\tau_0,\mu 0,\phi_0)$ and $C_F^W(\tau_0)$ are stored in contf.cfw3i and contf.cfw3f, respectively.

3.5 Grey test case

If cmd.context is set to 'grey', a 3D ($n_x = n_y = 10$) hydrostatic atmosphere is constructed, instead of reading a 3D model. The temperature stratification on the Rosseland optical depth scale is given by

$$T(\tau_{\text{Ross}}) = T_{\text{eff}} \left(\frac{1}{2} + \frac{3}{4}\tau_{\text{Ross}}\right)^{1/4}$$
 (62)

and the source function is linear in τ_{Ross} :

$$S(\tau_{\text{Ross}}) = \frac{\sigma}{\pi} T_{\text{eff}}^4 \left(\frac{1}{2} + \frac{3}{4} \tau_{\text{Ross}} \right). \tag{63}$$

The Eddington-Barbier relation is strictly correct in this case. For any inclination $\mu = \cos \theta$, the emergent continuum intensity is given by

$$I_c(\mu) = \frac{\sigma}{\pi} T_{\text{eff}}^4 \left(\frac{1}{2} + \frac{3}{4} \mu \right).$$
 (64)

In particular, at disk-center ($\mu = 1$) the continuum intensity is

$$I_c(\mu = 1) = \frac{5}{4} \frac{\sigma}{\pi} T_{\text{eff}}^4,$$
 (65)

and the flux is

$$F_c = 2\pi \int_0^1 \mu I_c(\mu) \, \mathrm{d}\mu = \sigma T_{\text{eff}}^4.$$
 (66)

Comparison of the results obtained from LINFOR3D for continuum intensity and flux for

TEFF = 5000.00, GRAV = 316.200

LUTAU1 = -8.0000000, LUTAU2 = 2.0000000, DLUTAU = 0.0800000

OPAFILE = 't5000g250mm30_marcs_idmean3xRT3.opta',

GASFILE = 'gas_cifist2006_m30_a04_15.eos',

EOSFILE = 'eos_cifist2006_m30_a04_l5.eos'

with the above theoretical results yields (LINFOR3D 3.1.3):

ratio			ntheta		
numerical / analytical	1	2	3	-3	4
$I_c(\text{linfor3D})/I_c(\text{Eq.}(65))$	1.0005573	1.0005573	1.0005573	1.0005573	1.0005573
$F_c(\text{linfor3D})/F_c(\text{Eq.}(66))$	1.0004105	1.0148776	1.0079553	1.0004507	1.0050481

If the ratio η of line opacity, κ_{ℓ} and continuum opacity, κ_{c} is constant with optical depth ($\eta = \kappa_{\ell}/\kappa_{c}$), the intensity in the line is simply

$$I_{\ell}(\mu) = \frac{\sigma}{\pi} T_{\text{eff}}^4 \left(\frac{1}{2} + \frac{3}{4} \frac{\mu}{1+\eta} \right),$$
 (67)

the **absolute** line depression is

$$D_I(\mu) = I_c(\mu) - I_\ell(\mu) = \frac{\sigma}{\pi} T_{\text{eff}}^4 \frac{3}{4} \mu \frac{\eta}{1+\eta}, \tag{68}$$

and the **relative** line depression at disk-center is

$$D_I(\mu = 1)/I_c(\mu = 1) = \frac{3}{5} \frac{\eta}{1+\eta}$$
 (69)

The absolute line depression for flux is

$$D_F = F_c - F_\ell = 2\pi \int_0^1 \mu D_I(\mu) \,\mathrm{d}\,\mu = \sigma T_{\text{eff}}^4 \frac{1}{2} \frac{\eta}{1+\eta} \,, \tag{70}$$

and the relative line depression for flux is

$$D_F/F_c = \frac{1}{2} \, \frac{\eta}{1+\eta} \,. \tag{71}$$

The ratio between the relative line depression in flux and at disk-center is therfore 5/6, and the same ratio holds for the equivalent widths.

The local absorption line profile is now defined by

$$\eta(\alpha, v) = \eta_0 H(\alpha, v), \tag{72}$$

3.5 Grey test case

where $v = (\lambda - \lambda_0)/\Delta \lambda_D$, and $\alpha = \Delta \lambda_N/2/\Delta \lambda_D$ ($\Delta \lambda_D$: Doppler width, $\Delta \lambda_N$: full width at half maximum of the Lorentzian damping profile). The 'Voigt function' $H(\alpha, v)$ is normalized such that (for $\alpha \ll 1$), $H(\alpha, v) = 0 \approx 1$. Assuming that η_0 , α , and $\Delta \lambda_D$ are constant, we can compute the emergent line profile from Eq. (69) or (71). At disk-center, we have

$$D_I(\mu = 1)/I_c(\mu = 1) = R_I = \frac{3}{5} \frac{\eta_0 H(\alpha, v)}{\eta_0 H(\alpha, v) + 1},$$
(73)

and for flux

$$D_F/F_c = R_F = \frac{1}{2} \frac{\eta_0 H(\alpha, v)}{\eta_0 H(\alpha, v) + 1}.$$
 (74)

Clearly, the emergent line profiles are no longer Voigt profiles due to saturation effects.

The (reduced) disk-center equivalent width is obtained from numerical integration of the emergent line profile:

$$\tilde{W}_I = \int_{-\infty}^{+\infty} R_I(v, \eta_0, \alpha) \, \mathrm{d} v \,, \tag{75}$$

and $\tilde{W}_F = 5/6 \, \tilde{W}_I$. An 'analytical' Curve-of-Growth, $\tilde{W}(\eta_0; \alpha = 0.01)$ is shown in Fig. 1.

The equivalent width in [mA] is obtained from the reduced equivalent width by

$$W_{\lambda}[\mathbf{m}\mathring{\mathbf{A}}] = 1000 \,\lambda_0[\mathring{\mathbf{A}}] \,\frac{\Delta v_D}{c} \,\tilde{W} \,. \tag{76}$$

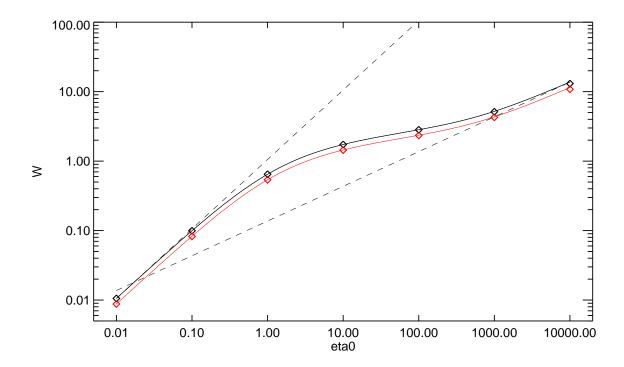


Figure 1: Analytical Curve-of-Growth showing the (reduced!) equivalent width (integrated from v = -100 to v = +100) as a function of η_0 , assuming $\alpha = 0.01$. **Black**: disk-center, **red**: flux. The dashed lines have slopes 0.5 and 1.0. Diamonds show the numerical results obtained with LINFOR3D (integration from v = -50 to v = +50).

The results of a number of test calculations are listed below. The wavelength resolution was chosen to be 1/10 of the Doppler width: $\delta\lambda = 0.1 \lambda_0 \Delta v_D/c$. The wavelength range was set to ±50 Doppler widths; $\Delta v_D = 6$ km/s, $\alpha = 0.01$. The line file used for the test calculations is shown below.

```
alam
        Vdop
                 eta0
                         avgt
                                 dlam
                                         ddlam
    7
       grey sf Vdop=2.D-5, eta0=1.0D-2, avgt=1.D-2
Test
1 7
                          1.0D-2 4.00D0 0.80D-2
4000.000 2.0D-5
                 1.0D-2
       grey sf Vdop=2.D-5, eta0=1.0D-1, avgt=1.D-2
Test
1 7
4000.000 2.0D-5
                 1.0D-1 1.0D-2 4.00D0 0.80D-2
Test
       grey sf Vdop=2.D-5, eta0=1.0D0, avgt=1.D-2
                          1.0D-2 4.00D0 0.80D-2
4000.000 2.0D-5
                 1.0D0
                Vdop=2.D-5, eta0=1.0D1, avgt=1.D-2
Test
       grey sf
1 7
4000.000 2.0D-5
                 1.0D1
                          1.0D-2 4.00D0 0.80D-2
       grey sf Vdop=2.D-5, eta0=1.0D2, avgt=1.D-2
Test
   7
4000.000 2.0D-5
                 1.0D2
                          1.0D-2 4.00D0 0.80D-2
Test
       grey sf Vdop=2.D-5, eta0=1.0D3, avgt=1.D-2
  7
4000.000 2.0D-5
                 1.0D3
                          1.0D-2 4.00D0 0.80D-2
       grey sf
                Vdop=2.D-5, eta0=1.0D4, avgt=1.D-2
Test
1 7
4000.000 2.0D-5
                 1.0D4
                         1.0D-2 4.00D0 0.80D-2
clam
           gfscale
-4000.000
           1.0
```

For the following tabulations we have defined

$$\Delta W_I = \log_{10} W_I(\text{linfor3D}) - \log_{10} W_I(\text{Eq.}(75)),$$
 (77)

and

$$\Delta W_F = \log_{10} W_F(\text{linfor3D}) - \log_{10} \frac{5}{6} W_I(\text{Eq.}(75)), \tag{78}$$

These results are obtained with intline=1:

$\overline{\eta_0}$	ΔW_I		ΔW_F	
	[dex]	ntheta=-3	ntheta=3	ntheta=4
1.0E-02	+0.000342	+0.000336	-0.002949	-0.001690
1.0E-01	+0.000331	+0.000327	-0.002958	-0.001698
1.0E+00	+0.000269	+0.000271	-0.003014	-0.001755
1.0E+01	+0.000072	+0.000081	-0.003203	-0.001942
1.0E+02	-0.000820	-0.000807	-0.004088	-0.002831
1.0E+03	-0.005441	-0.005432	-0.008714	-0.007456
1.0E+04	-0.021428	-0.021421	-0.024704	-0.023446

These results are obtained with intline=-2:

$\overline{\eta_0}$	ΔW_I		ΔW_F	
	[dex]	ntheta=-3	ntheta=3	ntheta=4
1.0E-02	+0.000334	+0.000328	-0.002957	-0.001698
1.0E-01	+0.000324	+0.000320	-0.002965	-0.001706
1.0E+00	+0.000261	+0.000263	-0.003022	-0.001762
1.0E+01	-0.000063	+0.000074	-0.003211	-0.001950
1.0E+02	-0.000825	-0.000814	-0.004097	-0.002838
1.0E+03	-0.005447	-0.005438	-0.008720	-0.007463
1.0E+04	-0.021432	-0.021425	-0.024708	-0.023450

4 Program Files and Data input files

In this section all the program files making up the LINFOR3D package are listed. First an overview on the program flow and the structures in common block linfordata is given. The format of the data input files is described since the primary way the user controls the program execution is via the control parameters read from linfor_setcmd.pro (see Section 5). The line parameters are specified in the input file line.dat (see Section 6).

4.1 Main program flow

Basically, the calling sequence is as follows (incomplete listing of linfor_3D.pro):

- Read input parameters (linfor_setcmd.pro)
- Initialize atomic data (linfor_atom.pro)
- Read line data: (linfor_rdline.pro)
- Initialize ionopa abundances, opacity tables and EOS tables
- Set constants (linfor_init)
- Define ff, type linfor_flowfield (linfor_flowfield__define.pro)
- Define f1, type linfor_flowfield: (linfor_flowfield__define.pro)
- Define fx, type linfor_flowfield: (linfor_flowfield__define.pro)
- Define ss, type linfor_spectrum: (linfor_spectrum__define.pro)
- Define s1, type linfor_spectrum: (linfor_spectrum__define.pro)
- Define sx, type linfor_spectrum: (linfor_spectrum_define.pro)
- Read model data into ff structure (linfor_rduio.pro)
- Recompute model on refined z-grid (linfor_regrid.pro)
- Compute ionopa quantities (pe, kappa, zeta) and monochromatic tau for 3D model (linfor_ionopa_3d.pro)
- Construct 1D reference atmosphere from ff, store in f1: (linfor_refatm.pro)
- Compute ionopa quantities (pe, kappa, zeta) and monochromatic tau for 1D reference atmosphere (linfor_ionopa_3d)
- Do radiative transfer calculations for 3D model (linfor_dort.pro)
- Do radiative transfer calculations for averaged 3D atmosphere (linfor_dort.pro)
- Store results for later evaluation (linfor_eval, ss, s1, nf, kl)
- Make Plots of line profiles and bisectors (linfor_plot1.pro)
- Do radiative transfer calculations for 1D reference atmosphere (linfor_dort.pro)
- Store results for later evaluation (linfor_evalx.pro)
- Create postcript file(s) (linfor_plot2.pro)
- Generate output files linfor_3D_1.uiosave and linfor_3D_2.uiosave (uio_save.pro).

- (Generate linfor_3D_3.uiosave if cc3d_flag=1.)
- (Generate linfor_3D_1X.uiosave if run_flag=-3.)
- Free pointers to structures ff, f1, fx, ss, s1, and sx if free_flag = 1 (see Sect. 5.1) (linfor_flowfield_free.pro)

4.2 Structures in Common Block linfordata

Table 1 shows a list of the structrues in common block 'linfordata' used by the linfor_3D package.

Structure	Defined in	Description
atom	linfor_atom.pro	Atomic weights & ionization potentials
const	linfor_init.pro	Physical & model constants
cmd	linfor_setcmd.pro	Input parameters controlling program execution
line	linfor_rdline.pro	Line data derived from 'line.dat'
gas	linfor_init.pro	GAS tables initialized by 'tabinter_rdcoeff'
eos	linfor_init.pro	EOS tables initialized by 'tabinter_rdcoeff'
result	linfor_init.pro	Basic results for computing abundance corrections

Table 1: List of all structures in common block 'linfordata': the table shows the name of the structure, the routine where it is defined, and a description. A brief description of the arrays/sub-structures contained within each structure is given in Sect. 7.

4.3 IDL/GDL Files

Table 3 shows a list of all source files necessary to run LINFOR3D. Finally, you will also need the files which are listed in Table 2:

File name	Type	Description
blam.pro	F	Computes the Kirchhoff-Planck function.
monocubic.pro	F	Performs monotonic piecewise cubic interpolation.
ms_int.pro	F	Integrates a given function over optical depth.

Table 2: List of additional IDL modules which are not unique to LINFOR3D.

All versions of LINFOR3D require the UIO library to handle the I/O of the CO⁵BOLD files, and versions 6.0.0 require them for ALL I/O done during the programflow.

File name	Type	Description
linfor_3D.pro	S	main program
linfor_flowfielddefine.pro	S	Definition of flow field structure
linfor_spectrumdefine.pro	S	Definition of spectrum structure
linfor_raysysdefine.pro	S	Definition of ray system structure
linfor_atom.pro	S	Defines atomic data
linfor_setwts.pro	S	Defines weights for angle quadrature (retired after version 6.2.7)
linfor_setwts_lobatto.pro	S	Replacement for linfor_setwts.pro. Further explanations given in Sect. 5.9
linfor_setwts_dblgaus.pro	S	Additional definition for angle quadrature. See Sect. 5.9

4.3 IDL/GDL Files 21

linfor_setwts_dblrdau.pro	S	Additional definition for angle quadrature. See Sect. 5.9
linfor_setwts_special.pro	S	Special definition for angle quadrature. See Sect. 5.9
linfor_setcmd.pro	S	Command file, parameter input
linfor_rdxatm.pro	S	Reads 1D reference atmosphere,
-		calling linfor_rdatmos, linfor_rdatlas9,
		linfor_rdmarcs, rdl50 or linfor_rdfalmod
linfor_rdatlas9.pro	S	Reads ATLAS9 1D atmosphere (atm.dat)
linfor_rdmarcs.pro	S	Reads MARCS 1D atmosphere (atm.dat)
linfor_rdfalmod.pro	S	Reads FAL 1D atmosphere (atm.dat)
linfor_rdatmos.pro	S	Reads ATMOS 1D atmosphere (atm.dat)
linfor_rdf15.pro	S	Reads a sequence of FOR15 snapshots
		from 2D Kiel hydro simulations (FOR15)
linfor_rdsav.pro	S	Reads 3D snapshot from Copenhagen code (savfs)
linfor_rduio.pro	S	Reads 3D snapshot from CO ⁵ BOLD uio output files
linfor_rdvog.pro	S	Reads 3D snapshot from Voegler MHD code
linfor_findff.pro	S	Finds cached flow fields
linfor_rdline.pro	S	Reads line data (line.dat)
linfor_init.pro	S	Initializes ionopa, EOS, Opacities, several constants
linfor_bisector.pro	S	Computes line bisector positions
1		called by linfor_plot1 and linfor_plot2
linfor_convol.pro	S	Convolves line profile with Gauss kernel
_ •		called by linfor_plot1 and linfor_plot2
linfor_dort.pro	S	Computes spectrum from flow field
		(main RT module calling several lower level routines)
linfor_eval.pro	S	Evaluates mean spectrum, "abundance corrections"
linfor_evalx.pro	S	Evaluates reference spectrum, "abundance correc-
		tions"
linfor_incline.pro	S	Inclines 3D flow field, called by linfor_ztau
linfor_ionopa_3d.pro	S	Calculates electron pressure, ionization fractions,
		and monochromatic optical depth for given flow field
linfor_rad3.pro	S	Integration of RT equation
linfor_refatm.pro	S	Define 1D reference atmosphere from 3D flow field
linfor_regrid.pro	S	Cut out surface layers from original model, re-define
		grid
linfor_tauinfo.pro	S	Prints information about optical depth scales
linfor_ztau.pro	S	Prepares bundle of (inclined) rays on monochromatic
		tau
linfor_plot0.pro	S	Plots flow field
linfor_plot1.pro	S	Plots spatially resolved line profiles
linfor_plot2.pro	S	Plots averaged line profiles
(linfor_plot3.pro)	S	Plots monochromatic granulation images
alpha_line.pro	F	Computes α -parameter for VOIGT function
eta0.pro	F	Computes η_0 , the opacity at line center of metal lines
rrca.pro	F	Computes mean square orbital radius of electron
		(Unsöld)
vdop.pro	F	Computes (thermal+turbulent) Doppler velocity $[c_s]$
linfor_timing.pro	S	Prepares and gathers timing statistics
linfor_timing_print.pro	S	Print timing statistics
uio_save.pro	S	UIO formatted save procedure
uio_restore.pro	S	UIO formatted restore procedure

Table 3: List of all IDL modules: the table shows the file name, the type (Subroutine or Function, and its description.

5 Parameter Input: linfor_setcmd.pro

The input parameters (except for those defined in line.dat, see Sect. 6) are basically specified by editing the routine linfor_setcmd.pro. In this way, the user defines the structure cmd (see Table 1). The order of entries is irrelevant. Parameters which are not required may be omitted.

A detailed explanation of the various input parameters and their possible values is given in the following sections. An example follows in Sect. 5.11.

5.1 Program execution flags

The user can control the program execution by setting the flags run_flag, nlte_flag, cv1_flag, cv2_flag, cv3_flag, plt_flag, maps_flag, cc3d_flag, rdbb_flag, free_flag, which are explained in more detail below.

```
function: program mode
required: always
type: integer
values: -3, -2, -1, 0, 1, 2, 3 (usually 3)
```

This parameter determines the general function of LINFOR3D:

Setting run_flag = -3 allows you to compute the external 1D atmosphere only. While a snap-shot is still required to run Linfor3D correctly, no 3D or (3D) data is computed or written to file. The results are stored in the structure 'linfor_1X.uiosave'. N.B. mode is only available from version 6.1.0 onwards.

Setting run_flag = -2 allows you to compute 3x3 file for the external reference model only.

Setting Setting $run_flag = -1$ allows you to restore old results, and replace the results of the previous 1D external atmosphere with those of a different 1D external atmosphere.

Setting run_flag = 0 (similar to run_flag = -1) allows you to quickly compare the 3D spectra with another external 1D reference atmosphere. Finally, the results are saved in files 'linfor_3D_1.uiosave' and 'linfor_3D_1.uiosave'. Rarely used setting.

Setting run_flag = 1 is used for plotting the structure of the input model on the original grid. No radiative transfer calculations are done.

Setting run_flag = 2 is used for plotting the structure of the input model on the reduced (refined) grid. No radiative transfer calculations are done.

Setting run_flag = 3 is the usual case. After construction of the 3D atmosphere on the reduced (refined) grid and of the 1D mean atmosphere, the line formation calculations are done, and the results are plotted ('linfor_plot1': spatially and temporally resolved line profiles and bisectors, 'linfor_plot2': surface and time averaged line profiles and bisectors). Finally, the results are saved in files 'linfor_3D_1.uiosave' and 'linfor_3D_2.uiosave'.

run_flag value		control of program flow
-3	:	load 3D models, (compute 1D ref. spectrum), save results
-2	:	compute 1D 3x3 external atmosphere
-1	:	restore results, (compute 1D ref. atmosphere & spectrum),
		save results
0	:	restore results, (compute 1D ref. atmosphere & spectrum),
		plot2, save results
1	:	compute 3D, 1D atmospheres (1), plot01, stop
2	:	compute 3D, 1D atmospheres (1,2), plot02, stop
3	:	compute 3D, 1D atmospheres (1,2), line formation,
		plot1, plot2, save results

5.1.2 cv1_flag function : enforce $\langle \rho u_x \rangle = 0$ required : always type : integer values : 0, 1

The parameter cv1_flag controls whether or not the *x*-component of the velocity field is adjusted to ensure zero mass flux in *x*-direction. (0: no, 1: yes). Default 0

```
5.1.3 cv2_flag

function : enforce \langle \rho u_y \rangle = 0
required : always
type : integer
values : 0, 1
```

The parameter $cv2_flag$ controls whether or not the *y*-component of the velocity field is adjusted to ensure zero mass flux in *y*-direction. (0: no, 1: yes). Default 0

```
5.1.4 cv3_flag

function : enforce \langle \rho u_z \rangle = 0
required : always
type : integer
values : 0, 1
```

The parameter cv3_flag controls whether or not the z-component of the velocity field is adjusted to ensure zero mass flux in z-direction. (0: no, 1: yes). Default 0

5.1.5	plt_flag		
	function	:	plotting of bisectors
	required	:	always
	type	:	integer
	values	:	-1, 0, 1

The parameter plt_flag controls if line bisctors should be plotted or not (0: no, 1: yes). If plt_flag is set to -1, all plotting is suppressed.

5.1.6	maps_flag			
	function	:	controls output of intensity maps	
	required	:	always	
	type	:	integer	
	values	:	0, 1, 2	

The parameter maps_flag controls the output of intensity maps which are provided in the IDL structure MAPS:

value		meaning
0	:	Continuum images only. Create map ICLAMO.
1	:	Continuum images (ICLAMO) plus images at the centre of the wavelength window
		(ICLAM1), all at wavelength $\lambda = clam$;
2	:	Continuum images (ICLAM0) plus images (ICLAM2) at all wavelengths within the
		wavelength window of width 2 · dlam around the central wavelength clam:
		$\lambda_i = clam - dlam + i \cdot ddlam $ (see Sect. 6);

5.1.7	cc3d_flag		
	function	:	output of 3D contribution function
	required	:	always
	type	:	integer
	values	:	0, 1

The parameter cc3d_flag controls whether the 3D continuum intensity contribution function should be saved in structure contf3d or not (0: no, 1: yes).

5.1.8	nlte_flag		
	function	:	output of 3D contribution function
	required	:	always
	type	:	integer
	values	:	0, 1, 2, 3

The parameter nlte_flag controls whether the line transfer is performed in LTE (nlte_flag=0) or in NLTE (nlte_flag=1, 2, 3). The NLTE options work only for lines with available departure coefficients, which are read from a separate data file (see below).

value		meaning
0	:	Continuum and lines in LTE.
1	:	Continuum in LTE, line source function in LTE, line opacity in NLTE
2	:	Continuum in LTE, line opacity in LTE, line source function in NLTE,
3	:	Continuum in LTE, line opacity and source function in NLTE

function : free pointers in structures at end of program required : always type : integer values : 0, 1

If free_flag = 1, then each run of LINFOR3D allocates fresh memory for the structures ff, f1, fx, ss, s1, and sx. In this case the corresponding pointers are removed at the end. If you want to examine the structures after the end of execution, you must have free_flag = 0. If you want to run the program several times in a row with different input parameters, you should set free_flag = 0 in order to avoid additional memory allocation for each run.

5.2 General paths

function : directory where '.abu' files and 'atom.dat' are located required : always type : string values : e.g. '/home/mst/ABU/'

If abupath is not specified in the command file, the path is taken from environment variable '\$LINFOR3D_ABU'.

5.2.2	ff_path		
	function	:	directory to be used for reading and writing cached flow fields
	required	:	always
	type	:	string
	values	:	e.g. '/data/mst/ffcache/'

5.2.3	opapath		
	function	:	directory with opacity tables (.opta files)
	required	:	always
	type	:	string
	values	:	e.g. '/home/mst/RHD/opa/dat/'

We recommend setting the environment variable \$OPTABLES

5.2.4	gaspath		
	function	:	directory with GAS tables (gas_*.eos files)
	required	:	always
	type	:	string
	values	:	e.g. '/home/mst/RHD/eos/dat/'

5.3 Model data 27

5.2.5	eospath		
	function	:	directory with EOS tables (eos_*.eos files)
	required	:	always
	type	:	string
	values	:	e.g. '/home/mst/RHD/eos/dat/'

We recommend setting the environment variable \$EOSTABLES for these two paths.

5.3 Model data

5.3.1	context		
	function	:	source of input model
	required	:	always
	type	:	string
	values	:	e.g. 'cobold'

value		meaning
'cobold'	:	3D CO⁵BOLD
'copenhagen'	:	N&S 3D code
'kiel'	:	Kiel 2D HDW-Code
'muram'	:	MURAM 3D MHD Code
'grey'	:	construct grey 3D $(n_x = n_y = 10)$
	:	hydrostatic atmosphere for test purposes

The τ_{Ross} grid of the grey atmosphere is defined by the parameters cmd.lutau1, cmd.lutau2, cmd.dlutau. The atmospheric parameters must be specified as cmd.Teff and cmd.grav. The opacity table must be specified as cmd.opafile, and the equation of state as cmd.eosfile and cmd.gasfile.

5.3.2	rhdpath		
	function	:	directory with 2D/3D model atmospheres (.end, .full files)
	required	:	always
	type	:	string
	values	:	e.g. '/data/mst/model/'

5.3.3	modelid		
	function	:	name of 2D/3D model file
	required	:	always
	type	:	string
	values	:	e.g. 'gt57g44n66_3Dgz.end'

Note: A list of files can be specified by using wildcards, e.g. 'chro3D04*.full'.

function : full path to parameter file (rhd.par) required : CO⁵BOLD only type : string values : e.g. '/data/mst/model/par/gt57g44n66.par'

function : full path to xbc files (*.xbc) required : CO⁵BOLD only type : string values : e.g. '/data/mst/NLTE3D_data/model/'

Note: xbc-files are necessary for NLTE line formation calculations. Presently limited to Li for selected CO⁵BOLD models.

5.3.6	abuid		
	function	:	Model abundance mixture to be used in the ionopa (or ionopa2) routine
	required	:	always
	type	:	string
	values	:	'kiel', 'cifist2006', 'special'

abuid identifies the solar abundance mix which is then modified according to dmetal and dalpha (see below). The corresponding tables, kiel.abu, cifist2006.abu, or special.abu must be located in directory abupath. Version 6.2.2 onwards use ionopa2, which requires two abundance mixture files: The model abundance mixture, abuid (above); and the spectrum abundance mixture, abuidx (below).

5.3.7	abuidx		
	function	:	Spectrum abundance mixture to be used in ionopa2 routine
	required	:	always (version 6.2.2 onwards)
	type	:	string
	values	:	'kiel', 'cifist2006', 'special'

LINFOR3D has an additional way it computes ionopa quantities (pe, kappa, zeta) and the monochromatic tau scale. When abuid=abuidx (or if abuidx is **not** defined), these quantities are computed as they were in previous versions of LINFOR3D. When abuid contains the solar abundance mixture of the CO⁵BOLD model and abuidx contains the desired abundance mixture of the spectrum synthesis then ionopa2 computes the quantities twice to compensate for the change in abundance.

5.3.8	dmetal		
	function	:	metallicity [M/H] (log ₁₀) to be used in ionopa-routines
	required	:	always
	type	:	float
	values	:	e.g. 0.0, -0.5, -2.0

The logarithmic abundance of all elements beyond Li (N > 3) is changed by dmetal.

function : alpha enhancement to be used in ionopa-routines required : always type : float values : e.g. 0.0, +0.4

The logarithmic enhancement factor to be applied to all α -elements.

LINFOR3D considers O, Ne, Mg, Si, S, Ar, Ca, and Ti as α -elements.

```
function : sampling of model in x-direction required : if context='cobold', 'kiel', 'muram' type : integer values : 1, 4, 10; -1
```

If both nx_skip and ny_skip (see Sect. 5.3) are negative, the original data are re-binned from (nx,ny) to (nx/abs(nx_skip), ny/abs(ny_skip)). In the usual case that both nx_skip and ny_skip are positive, the original data are re-sampled, skipping by nx_skip in x, and by ny_skip in y-direction (nx/nx_skip, and ny/ny_skip should preferably be an integer). If nx_skip and ny_skip have different signs, an error message is printed and the program is stopped. The value 1 has no effect.

5.3.11	ny_skip		
	function	:	sampling of model in x-direction
	required	:	<pre>if context='cobold','kiel','muram'</pre>
	type	:	integer
	values	:	1, 4, 10; -1

For details see description of nx_skip (Sect. 5.3).

5.4 More model information (MOST read from parameter file for CO⁵BOLD data)

The *majority* of parameters in this section are ignored in the case of CO⁵BOLD data and instead read from the specified CO⁵BOLD parameter file. Please read this section carefully to avoid errors in your synthesis.

5.4.1	opafile		
			name of opacity file (binned opacity tables) not needed if context='cobold'
	type values	:	string e.g. 'g2v.opta'

function : name of GAS file $(P, T \to \rho, e, ...)$ required : not needed if context='cobold' type : string values : e.g. 'gas_mm00_l.eos'

5.4.3	eosfile		
	function	:	name of EOS file $(\rho, e \rightarrow P, T,)$
	required	:	not needed if context='cobold'
	type	:	string
	values	:	e.g. 'eos_mm00_1.eos'

5.4.4	htau0		
	function	:	opacity scale height [cm] at top of 3D model
	required	:	always
	type	:	float
	values	:	e.g. $60.0E5$; default = 0.0

A **default value of 0.0** tells LINFOR3D to take this parameter from the parameter file (set at sect. 5.3 - parfs - e.g. rhd.par).

5.4.5	qmol		
			mean molecular weight of neutral gas not needed if context='cobold'
	type	:	float
	J 1		e.g. 1.301855

Important Note: This parameter has been retired in LINFOR3D version 6.2.6 onwards.

5.4.6	Teff	
	required type	: effective temperature of 3D model : not needed if context='cobold' : float : e.g. 5770.0

```
function : surface gravity [cm/s²] of 3D model
required : not needed if context='cobold'
type : float
values : e.g. 27500.0
```

function : surface temperature ($\tau = 0$) of 3D model is tsurffac· $T_{\rm eff}$ required : always type : float values : e.g. 0.727903; **default = 0.0**

A **default value of 0.0** tells LINFOR3D to take this parameter from the parameter file (set at sect. 5.3 – parfs – e.g. rhd.par). This only affects **LINFOR3D** version 6.2.6 onwards. Versions of LINFOR3D older than this do not read this parameter from setcmd if context='colbold'.

5.5 Model data - reading of 'full' files (CO⁵BOLD only)

The parameters in this section are only needed for reading snapshot from CO⁵BOLD data files.

function: first snapshot to be read from full file(s) required: only needed if context='cobold' type: integer values: 1

5.5.2	isnap_full_2		
			last snapshot to be read from full file(s)
	required	:	only needed if context='cobold'
	type	:	integer
	values	:	1

5.5.3	istep_full		
	function	:	step for reading snapshots from full file(s)
	required	:	only needed if context='cobold'
	type	:	integer
	values	:	1

5.6 $\langle 3D \rangle$ mean model

5.6.1 mavg function : mode of averaging 3D T-structure on τ_{Ross} required : always type : integer values : 1, 4

value		meaning
1		$T_{\langle \text{3D} \rangle}(\tau_{\text{Ross}}) = \langle T_{\text{3D}}(\tau_{\text{Ross}}) \rangle$
4	:	$T_{\langle 3\mathrm{D}\rangle}(\tau_{\mathrm{Ross}}) = \langle T_{\mathrm{3D}}^4(\tau_{\mathrm{Ross}}) \rangle^{1/4}$

5.7 External 1D reference model

5.7.1	atmpath		
	function	:	directory with 1D model atmospheres
	required	:	always
	type	:	string
	values	:	e.g. '/home/mst/atm/'

5.7.2	atmfile		
	function	:	name of 1D reference model
	required	:	always
	type	:	string
	values	:	e.g. 'NONE', 'dxgt57g44n59.150', 'falc.at9', 'falc.mod', '<3D>'

Note: No external 1D reference atmosphere will be used if atmfile=`NONE'. In this case the parameter atmpath has no meaning. If atmfile=`<3D>' the external model atmosphere is replaced by a global $\langle 3D \rangle$ model atmosphere constructed by averaging the individual $\langle 3D \rangle$ snapshots.

LINFOR3D has the capability to read in several types of external 1D model atmospheres. The way it determines the type of model atmosphere is with the file extension. For example, '.150' is determined as an LHD model atmosphere. This is determined at the linfor_rdxatm.pro routine level. The result of that will invoke one of several routines to properly read the model atmosphere. Here is a list of 1D model atmospheres accepted by LINFOR3D, the routine name that reads the model, and what the external model atmosphere file extension should be:

Model atmosphere		Invoked routine		File extension
LHD	:	rdl50.pro	:	'.15 0 '
Kiel ATMOS	:	linfor_rdatmos.pro	:	'.atm'
ATLAS9	:	linfor_rdatlas9.pro	:	'.at9' or 'a12'
MARCS	:	linfor_rdmarcs.pro	:	'.mod'
FAL*	:	<pre>linfor_rdfalmod.pro</pre>	:	'.fal'

^{*}Fontenla, Avrett, Loeser models (1993, ApJ 406, 319)

Finally, should you wish to compute a $\langle 3D \rangle$ model again, for different parameters, such as microturbulence, the routine d3a21dx.pro will convert a standard $\langle 3D \rangle$ model (which is saved as an idlsave) to a properly formatted ATLAS9 model accepted by LINFOR3D. However, this model is only compatable with LINFOR3D and the routine is only available with LINFOR3D version 6.2.6 onwards.

33

5.8 Line data and radiative transfer

5.8.1 linfs

function : name of line data file

required : always type : string

values : e.g. 'Li67.line'

Note: If linfs is not specified, the default value 'line.dat' is assumed.

5.8.2 lutau1

function : smallest $\log \tau_{\rm Ross}$ covered by sub-model (refined z-grid)

required : always type : float

values : e.g. -7.0D0

5.8.3 lutau2

function : largest $\log \tau_{Ross}$ covered by sub-model (refined z-grid

required : always type : float values : e.g. 2.0*D*0

5.8.4 dlutau

function : z-spacing of sub-model corresponds roughly to $\Delta \log \tau_{\rm Ross}$ =dlutau

required : always type : float

values : e.g. 8.0D - 2

5.8.5 lctau1

function : smallest $\log \tau_{\rm cont}$ used for RT integration

required : always type : float

values : e.g. -7.0D0, ≥ 1 utau1

5.8.6 lctau2

function : largest $\log \tau_{\rm cont}$ used for RT integration

required : always type : float

values : e.g. 2.0D0, ≤ 1 utau2

5.8.7 dlctau

function : resolution in $\log \tau_{\rm cont}$ used for RT integration

required : always type : float

values : e.g. 8.0D - 2

function : controls broadening of hydrogen lines required : always type : integer values : 0, 1, 2, 3, 4

value meaning

0 : Cayrel & Traving (1960), default

1 : Resonance broadening: AG , Stark broadening: G

2 : Resonance broadening: BPO, Stark broadening: G

3 : Resonance broadening: A08 , Stark broadening: G

4 : Resonance broadening: A08 , Stark broadening: SH

AG: Ali & Griem (1966, Phys. Rev. 144, 366),

BPO: Barklem, Piskunov and O'Mara (2000, A&A 363, 1091),

A08: Allard et al. (2008, A&A 480, 581),

G: Griem (1960, ApJ 132, 883), with corrections to approximate the Vidal, Cooper & Smith (1973,

ApJS 25, 37) profiles.

SH: Stehlé & Hutcheon (1999 A&AS, 140, 93)

Note 1: option Hbrd = 2 has an effect **only on H** α , **H\beta**, **and H\gamma**, and Hbrd = 3 affects **only H** α ; all other hydrogen lines are treated according to option Hbrd = 1, unless Hbrd = 0.

Note 2: option Hbrd = 4 is not currently working (as of version 6.2.4 – check the readme file in the later versions of LINFOR3D for updates on this).

5.8.9	vsini		
	function	:	Sets $v \sin i$ value for all spectra in linfor_plot2.pro only
	required	:	always
	type	:	float
	values	:	e.g. 1.0

5.8.10	ximicx		
	function	:	isotropic Gaussian microturbulence velocity [km/s] for external
			1D reference model (added quadratically to thermal velocity)
	required	:	always
	type	:	float
	values	:	e.g. 1.0

5.8.11	ximic1		
	function	:	isotropic Gaussian microturbulence velocity $[km/s]$ for $\langle 3D \rangle$
			mean models (added quadratically to thermal velocity)
	required	:	always
	type	:	float
	values	:	e.g. 1.0

35

5.8.12 ximic3

function : isotropic Gaussian microturbulence velocity [km/s] for 2D/3D models

(added quadratically to thermal flow velocity)

required : always type : float values : e.g. 1.0

5.8.13 ximacx

function : Isotropic Gaussian macroturbulence velocity [km/s] for external

1D reference model (additional line broadening after line formation)

required : always type : float values : e.g. 1.6

5.8.14 ximac1

function : Isoptropic Gaussian macroturbulence velocity [km/s] for $\langle 3D \rangle$

mean models (additional line broadening after line formation)

required : always type : float values : e.g. 1.6

5.8.15 ximac3

function : Isotropic Gaussian macroturbulence velocity [km/s] for 2D/3D models

(additional line broadening after line formation)

required : always type : float values : e.g. 1.6

5.8.16 vfacx

function : the x-component of the hydrodynamical velocity field of the

2D/3D models is multiplied by this factor

required : always type : float values : e.g. 0.0, 1.0

5.8.17 vfacy

function : the y-component of the hydrodynamical velocity field of the

2D/3D models is multiplied by this factor

required : always type : float values : e.g. 0.0, 1.0 function : the z-component of the hydrodynamical velocity field of the

2D/3D models is multiplied by this factor

required : always
type : float
values : e.g. 0.0, 1.0

function : controls microturbulence in 1D Curve-of-Growth required : always type : integer values : 0, 1

Determines whether or not different microturbulence values should be used when computing the 1D Curve-of-Growth. 0: only one value, given by ximicx and ximic1, respectively; 1: sequence of microturbulence values defined by parameters xi_a, xi_b, xi_d (see below).

function : determines start value for microturbulence sequence required : always type : float values : e.g. 0.0, default: 0.5

function : determines end value for microturbulence sequence required : always type : float values : e.g. 2.0, default: 1.5

function : determines intervals of microturbulence sequence required : always type : float values : e.g. 0.1, default: 0.125

The microturbulence sequence is computed as $xi(i) = xi0 * (xi_a + i * xi_d)$, i=0 .. im, where xi0 is ximicx and ximic1, respectively, and $im=(xi_b - xi_a)/xi_d$.

function : determines the variation of the continuum required : always type : float values : e.g. 20.0, default: 0

if dclam=0, the continuum is treated as constant (default). Otherwise, the continuum is computed at 3 wavelength points, clam-dclam, clam, clam+dclam, where clam is the central wavelength (in Å) of the computed spectral range (see Sect. 6), and dclam is half the width of the specified spectral range (in Å). The continuum is computed by parabolic interpolation inside the spectral window. If the spectral range of the specified synthetic spectrum (which is defined by the parameters of the line file (see Sect. 6) exceeds a few Å, dclam should be set to match half the total spectral range.

5.8.24	intmode		
	function	:	mode of integration in routines ms_int_tau and ms_int_exp
	required	:	always
	type	:	integer
	values	:	0, 1

Determines the mode of integration in routines ms_int_tau and ms_int_exp, which can be linear (0) or monotonic and cubic (1, standard).

5.8.25	intline		
	function	:	mode of integrating the line transfer equation
	required	:	always
	type	:	integer
	values	:	1, 2, -1, -2

Determines the method of integrating the line transfer equation (see Section 3 for details). Default value is intline=1.

value		meaning
1	:	Line depression on fixed $\log \tau$ scale (Eq. 41)
2	:	Line depression on monochromatic τ scale (Eq. 36)
-1	:	Line intensity on fixed $\log \tau$ scale (Eq. 25)
-2	:	Line intensity on monochromatic τ scale (Eq. 26)

5.8.26	nchunk		
	function	:	rad.transfer is done in n_chunk "slices"
	required	:	always
	type	:	integer
	values	:	e.g. 2

Default is nchunk = 1, i.e. the whole model is processed as one block. For large models, it may be necessary to split the computation into several 'chunks' to save memory.

5.9 Angle quadrature schemes

By default, LINFOR3D requires the following information to compute the transfer equation over several ray angles.

function : number of θ -angles for which spectrum is computed required : always type : integer values : 0, 1, 2, 3, (-3), 4, 6, 8

0: Intensity spectrum, > 0: Intensity and flux spectrum;

function : number of ϕ -angles for integration of flux spectrum required : always type : integer values : no restriction, typically 4

function : view angle $\mu = \cos \theta$ required : always type : float values : 0.0 ... 1.0

If the parameter ntheta=0, then the spectrum and intensity maps are computed for inclination angle mu0 (= $\cos \theta_0$).

mu0= 1.0 corresponds to vertical rays, i.e. disk center view.

mu0= 0.0 corresponds to the very limb, but a value of mu0=0.0 will clearly not work.

function : view angle required : always type : integer values : 0, 1, 2, 3

The parameter kphi determines the direction from which the model is viewed:

value		meaning
0	:	rays emerge parallel to the x-axis, i.e. the model is viewed somewhere
		on the 'equator' between the left limb and disk center.
1	:	rays emerge parallel to the y-axis, i.e. the model is viewed somewhere
		on the 'meridian' between the lower limb and disk center.
2	:	rays emerge anti-parallel to the x-axis, i.e. the model is viewed somewhere
		on the 'equator' between the right limb and disk center.
3	:	rays emerge anti-parallel to the y-axis, i.e. the model is viewed somewhere
		on the 'meridian' between the upper limb and disk center.

Other (integer) values of kphi are allowed, but give no new results; increasing kphi by one in-

creases phi by $\pi/2$.

However, since the release of LINFOR3D version 6.3.0, several new schemes have been introduced for the user to select:

Name		meaning
Lobatto	:	quadrature through routine linfor_setwts_lobatto.pro
Double Gauss	:	quadrature through routine linfor_setwts_dblgaus.pro
Double Gauss-Radau	:	<pre>quadrature through routine linfor_setwts_dblrdau.pro</pre>
Custom-made	:	quadrature through routine linfor_setwts_special.pro

These new quadrature schemes can be used by selecting them in the setcmd:

5.9.5	raybase		
	function	:	quadrature scheme
	required	:	always
	type	:	string
	values	:	'lobatto', 'dblgaus', 'dblrdau', and 'special'

If the raybase option is missing from the setcmd then the default lobatto is selected. For the user, little has changed. One must still select the number of μ and ϕ angles to use, like before. The only exception to this, is when the user elects to use a custom angle quadrature scheme.

To use the special case, a file called 'special.xmu' that contains the list of mu-angles and corresponding weights must be made available in the working directory. Examples of this file can be found in the Data subdirectory of the LINFOR3D directory tree.

5.10 Curve-of-Growth computations

As standard, LINFOR3D computes a Curve-of-Growth (CoG) for the 1D external and $\langle 3D \rangle$ model atmospheres. The range in abundance, and the sampling of the range were fixed within LINFOR3D. Version 6.2.5 onwards now includes the option to tailor the Curve-of-Growth, or deactivate the computations.

5.10.1	cog		
	function	:	Tailors the Curve-of-Growth computations
	required	:	always
	type	:	integer
	values	:	-1, 0, 1

Default is cog = 1. cog = 0 deactivates the CoG computations (speeds up computations of large line lists). cog = -1 activates a tailored CoG. Requires the three following parameters, otherwise Linfor3D computes a standard CoG (like cog = 1).

5.10.2	icg		
			sets index from default to user defined yes, if cog=-1
	type	:	integer e.g. 51, 101

function : sets minimum $\Delta \log gf$ value over which to perform CoG computations required : yes, if $\cos = -1$ type : float values : e.g. -3.0

function : sets maximum $\Delta \log gf$ value over which to perform CoG computations required : yes, if $\cos g - 1$ type : float values : e.g. +2.5

If these properties are not included in linfor_setcmd, the default settings are invoked; icg= 51, gflgmin= -1.0, gflgmax= +1.5.

All of the options defined in Sect. 5 are checked by linfor_checkcmd.pro and are set to default values in the event that they are missing from setcmd.

5.11 Example 41

5.11 Example

```
pro linfor_setcmd
common linfordata
```

```
cmd = $
;------
Prog-
lte_flag: w,
run_flag: 3, $
cv1_flag: 1, $
...? flag: 1, $
0, $
; Program execution flags:
                            ; 0 / 1 / 2 / 3: LTE or NLTE for lines with xb
nlte flag: 0. $
                             ; execution mode: -3, -2, -1, 0, 1, 2, 3
                             ; 0 / 1: enforce <rho*v1>(z)=0 off / on
                            ; 0 / 1: enforce <rho*v2>(z)=0 off / on
                            ; 0 / 1: enforce <rho*v3>(z)=0 off / on
                            ; -1 / 0 / 1: plotting off / bisectors off / on
 plt_flag: 1, $
                            ; create maps ICLAMO .. ICLAMm, m=map_flag
maps_flag: 1, $
cc3d_flag: 0, $
                            ; 0 / 1: output of CC3(nx,ny,nx) off / on
rdbb_flag: 0, $
                            ; 0 / 1: Read magnetic field, write SIR output
free_flag: 0, $
                             ; free pointers in structures at end of program
:------
; General paths:
abupath: getenv('LINFOR3D_ABU'), $
        ; Path to abu files and atom.dat
         ; if not set, abupath is read from environment variable LINFOR3D_ABU
ff_path: 'NONE', $
                                  ; directory with cached flow fields
                                    'NONE': do not use cached flow fields
opapath: getenv('OPTABLES'), $ ; directory with opacity tables
gaspath: getenv('EOSTABLES'), $ ; directory with GAS tables
eospath: getenv('EOSTABLES'), $ ; directory with EOS tables
:-----
; Model data:
context: 'cobold', $
rhdpath: '/data/models/d3gt57g44n59/bigsel/', $
                                              ; directory with model data
modelid: 'd3gt57g44n59.*.full', $ ; data file name
parfs: '/data/models/d3gt57g44n59/rhd.par', $ ; parameter file
xbcpath: '/data/models/d3gt57g44n59/NLTE3D/', $ ; directory of
                                                    departure coefficients
abuid: 'cifist2006', $ ; model abundance mixture, e.g. 'cifist2006' abuidx: 'special', $ ; spectrum abundance mixture, e.g. 'special'
dmetal: 0.0, $
                            ; log10 scaling for metal abundances (Z>3)
                           ; log10 scaling for alpha elements
dalpha: 0.0, $
                                  (O, Ne, Mg, Si, S, Ar, Ca, Ti)
nx_skip: 5, ny_skip: 5, $ ; sampling in x, y (kiel, cobold only)
; more information (all read from parameter file for CO5BOLD)
opafile: 'undefined', $
gasfile: 'undefined'. $
eosfile: 'undefined', $
teff: 5770.0, grav: 27500.0, $; grey, copenhagen, muram only
:-----
htau0: 0.0E0, $
tsurffac: 0.0E0, $
; Reading of 'full' files (CO5BOLD only):
                  ; first snapshot to be read from full file(s)
isnap_full_1: 1, $
                  ; last snapshot to be read from full file(s)
; step for reading snapshots from full file(s)
isnap_full_2: 9, $
istep_full: 2, $
```

```
; <3D> mean model:
mavg: 4, $; 1: T-average, 4: T^4-average for defining <3D> atmosphere
:-----
; External 1D reference model:
atmpath: '/data/models/d3gt57g44n59/lhdmodels/', $; directory of 1D
                                               reference model
atmfile: 'dxgt57g44n59.150', $
                                             ; name of reference model
                                               'NONE': no reference model
:-----
; Line data / radiative transfer:
linfs: 'line.dat', $ ; File with line data
lutau1: -7.0D0, lutau2: 2.0D0, dlutau: 8.0D-2, $ ; tau scale defining vertical
                                             model extent and resolution
lctau1: -7.0D0, lctau2: 2.0D0, dlctau: 8.0D-2, $; universal tau scale for
                                             integration of RT equation
ntheta: 3, nphi: 4, $ ; number of theta and phi angles mu0: 0.40, kphi: 0, $ ; view angle if ntheta=0 (cos theta,kphi*pi/2) n_chunk: 1, $ ; RT is done in n_chunk "slices"
; Curve-of-Growth control
      1, $ ; -1 / 0 / 1: Custom CoG / CoG off / default CoG calculations
         51, \$; number of points to compute COG over (used when cog = -1)
ica:
gflgmin: -1.0, $ ; minimum delta log(gf) (used when cog = -1)
gflgmax: +1.5, $ ; maximum delta log(gf) (used when cog = -1)
;-----
; Balmer line computation control
                            ; option for H line broadening
Hbrd: 3,$
                            ; 0 - (default)
                            ; Cayrel&Traving (self res.) + Griem (Stark)
                            ; 1 - Ali-Griem (self res.) + Griem (Stark)
                            ; 2 - BPO (self res.) + Griem (Stark)
                            ; 3 - Allard 08 (self res.) + Griem (Stark)
                             ; 4 - Allard 08 (self res.) + Stehle (Stark)
                            ; using properly convolved tabulated
; profiles
:-----
                           ; v sini (plot2); same for all spectra
vsini: 1.80, $
ximicx: 1.00, $
                            ; microturbulence [km/s], 1D-REF atmosphere
                            ; microturbulence [km/s], 1D-AVG atmosphere
ximic1: 1.00, $
ximic3: 0.00, $
                            ; microturbulence [km/s], 3D-RHD atmosphere
                            ; macroturbulence [km/s], 1D-REF atmosphere
ximacx: 1.60, $
                             ; macroturbulence [km/s], 1D-AVG atmosphere
ximac1: 1.60, $
                            ; macroturbulence [km/s], 3D-RHD atmosphere
ximac3: 0.00, $
vfacx: 1.00, $ vfacy: 1.00, $
                            ; fudge factor for 3D x-velocity
                            ; fudge factor for 3D y-velocity
vfacz: 1.00, $
                            ; fudge factor for 3D z-velocity
micro: 0, $
                            ; compute microturbulence sequence (0/1)
xi_a: 0.0, $
                             : microturbulence sequence start [km/s]
                             ; microturbulence sequence stop [km/s]
xi_b: 2.0,
           $
           $
                             ; microturbulence delta sequence [km/s]
xi_d: 0.1,
dclam: 0.0, $
              ; variation of continuum from clam-dclam .. clam+dclam [A]
intmode: 1, $
                             ; integration mode (linfor_msint)
intline: 1 $
                              ; line integration: depth (1,2) / I (-1,-2)
end
```

6 Line Data File: line.dat

There are several different formats (for historical reasons) to specify line data which are described in Sect. 6.2.

Note that all formats were extended in version 1.5.0 and now do have to contain the two lines

```
clam gfscale 2000.0 1.0
```

at the end. These parameters are explained in Sect. 6.1. Some helpful remarks concerning the conversion of line broadening parameters are given in Sect. 6.3.

A basic IDL program for creating a properly formatted line can be found in linfor_wrline.pro, within the Routines sub-directory within the LINFOR3D directory tree.

6.1 Parameters in Line Data File

function : continuum wavelength in Å, also center of wavelength window required : always type : float values : e.g., 2000.0

clam defines the wavelength where the continuum opacities are computed, and also defines the center of the window for which spectrum synthesis is done. The window extends from λ =clam-dlam to λ =clam+dlam, depending on the value of dlam specified for the particular line.

From Version 3.1.2, a **negative** clam indicates that the continuum source function is to be set to the wavelength-integrated Planck-Function, $S = \sigma T^4/\pi$, and the continuum opacity is set to the Rosseland mean opacity, $\kappa_{\rm cont} = \kappa_{\rm Ross}$..

```
function : global scaling factor for oscillator strengths
required : always
type : float
values : e.g., 1.0
```

Note: The value 1 has no effect. Useful when line.dat contains more than one transition.

6.2 Line Data Formats

6.2.1 Continuum only

It is possible to do pure continuum calculations. In this case, the line.dat file looks like this.

Example:

```
Some text header
1 1
Continuum, 2000 A
1 -1
clam gfscale
2000.0 1.0
```

Description of entries:

```
Row 1: Header (identifies the meaning of the columns for data in row 5)
```

Row 2: Two integers, kline and ktotal; both of them must be 1

Row 3: String, identifier of the continuum calculation

Row 4: Two integers, nbl = 1, incode = -1

Row 5: Description for data in row 6

Row 6: clam and gfscale (see Sect.6.1)

All the line parameters remain undefined.

6.2.2 Single line calculations, line data format '0'

For a **single unblended line**, the simplest form of the 'line.dat' file looks like this.

Example:

```
dlgC6
                                                                       ddlam
Mult
       namj
                  ei
                           alam
                                    gflg
                                                       drrca1 dlam
Fe I, 5500 A, 0.00 eV
       2600
                           5500.0
                                                               5.5D-1 5.5D-3
0000
                  0.000
                                    -6.000
                                              1.0
                                                       10.0
clam
         gfscale
2000.0
```

Description of entries:

```
Row 1: Header (identifies the meaning of the columns for data in row 5)
```

Row 2: Two integers, kline and ktotal

kline: number of line calculations requested in this file

ktotal: is the total number of spectral lines including blends

in this case kline = 1, ktotal = 1

Row 3: String, identifier of the (first) line calculation

Row 4: Integer *nbl*, integer array *incode*(*nbl*)

nb: number of blend components for this line calculation (= 1)

incode: integer array identifying the input format for each of the blend components (= 0)

Row 5: Line data in format '0' (7 + 2 columns):

C1: Multiplet number (for information only)

C2: Identifier of atom or ion (e.g. 2601 mean FeII)

C3: Excitation potential of lower level in [eV]

C4: Central wavelength of blend component

C5: $\log gf$ value of blend component

C6: $\Delta \log C_6$: Enhancement factor for van der Waals line broadening

C7: $\Delta r^2/a_0^2$: Difference of mean square electron orbital radii

C8: $\Delta\lambda$ [Å]: Line profile is computed from $\lambda_0 - \Delta\lambda$ to $\lambda_0 + \Delta\lambda$

C9: $\delta\lambda$ [Å]: Spacing of wavelength points for spectrum synthesis

(C10: W_0 [mÅ]: total equivalent width of this blend, see below)

Row 6: Description for data in row 6

Row 7: clam and gfscale (see Sect.6.1)

In this case, the Stark broadening (due to collisions with electrons) is neglected ($C_4 = 0$). Radiative damping (γ_{rad}) is treated in the classical approximation.

6.2 Line Data Formats 45

In the case of a single blended line the 'line.dat' file looks as follows:

Example:

```
dlgC6
                                                       drrca1 dlam
                                                                       ddlam
Mult
       namj
                  ei
                           alam
                                    gflg
1
Fe I, 0.00 eV + Fe II, 3.00 eV, 2000 A
    0 0
2
                  0.000
9999
       2600
                           2000.0
                                    -6.441
                                              1.0
                                                       10.0
                  3.000
                           2000.0
                                                       10.0
9999
       2601
                                    -4.550
                                              1.0
                                                               1.5D-1 1.5D-3
         gfscale
clam
2000.0
         1.0
```

Note that it is not necessary that the blend components belong to the same ion. Here kline = 1, ktotal = 2, nbl = 2, incode = [0, 0]. Note that only the last of the rows describing the blend need entries C8 and C9.

With a slight modification, it is possible to enter an **equivalent width** $(W_0 \text{ in } [m\text{Å}])$ in column C10. For this purpose, nbl must be negative, with |nbl| being the number of blend components. The gf value producing this equivalent width W_0 is returned in result.gflg01 (average 3D atmosphere) and result.gflg0x (1D reference atmosphere).

Example unblended line:

```
Mult
      namj chik
                     alam
                               gflg
                                        dlgC6 drrca1 dlam
                                                                ddlam
                                                                           M0
 1 1
                              0.000
                                                               10.00
                                                                        75.00 /
 N I Fictitious Line
                      1: /
                                       5500.0
                                              -7.6914 1.00
-1 0
9999
       700
             0.000
                     5500.0
                             -7.6914
                                      1.00
                                              10.00 3.00E-01
                                                               3.00E-03
                                                                           75.00
clam
         qfscale
2000.0
         1.0
```

Example blended line:

```
dlgC6 drrca1 dlam
Mult
       namj chik
                     alam
                                gflg
                                                                 ddlam
                                                                             W0
  1 2
Fe I, 0.00 eV + Fe II, 3.00 eV, 2000 A
-2 0 0
9999
       2600 0.000
                      2000.0
                               -6.441
                                        1.0
                                                10.0
9999
       2601 3.000
                     2000.0
                               -4.550
                                        1.0
                                               10.0
                                                     1.50D-1
                                                                1.50D-03
                                                                          100.00
         gfscale
clam.
2000.0
         1.0
```

6.2.3 Single line calculations, line data format '1'

For a **single unblended line**, the this form of the 'line.dat' file looks like this.

Example:

```
Mult
                      alam
                               gflg
                                        dlgC6 lu diu lo
                                                           dio
                                                                dlam
                                                                        ddlam
      nami
              ei
    1
O I ApJ Line 2: 92 6300.30 0.000 -9.773
  92
       800
               0.000
                      6300.30 -9.773
                                              1
                                                  0.0
                                                      2
                                                            0.0
                                                                4.D-1 4.D-3
                                        1.0
clam
         gfscale
2000.0
         1.0
```

Description of entries:

```
Row 1: Header (identifies the meaning of the columns for data in row 5)
```

Row 2: Two integers, kline and ktotal

kline: number of line calculations requested in this file

ktotal: is the total number of spectral lines including blends

in this case kline = 1, ktotal = 1

Row 3: String, identifier of the (first) line calculation

Row 4: Integer *nbl*, integer array *incode*(*nbl*)

nb: number of blend components for this line calculation (= 1)

incode: integer array identifying the input format for each of the blend components (= 1)

Row 5: Line data in format '1' (10 + 2 columns):

C1: Multiplet number (for information only)

C2: Identifier of atom or ion (e.g. 2601 mean FeII)

C3: Excitation potential of lower level in [eV]

C4: Central wavelength of blend component

C5: $\log gf$ value of blend component

C6: $\Delta \log C_6$: Enhancement factor for van der Waals line broadening

C7: LU: Orbital quantum number of valence electron of lower level

C8: DIU: excitation energy [eV] of parent term for lower level

C9: LO: Orbital quantum number of valence electron of upper level

C10: DIO: excitation energy [eV] of parent term for upper level

C11: $\Delta \lambda$ [Å]: Line profile is computed from $\lambda_0 - \Delta \lambda$ to $\lambda_0 + \Delta \lambda$

C12: $\delta\lambda$ [Å]: Spacing of wavelength points for spectrum synthesis

(C13: W_0 [mÅ]: total equivalent width of this blend, see below)

Row 6: Description for data in row 6

Row 7: clam and gfscale (see Sect.6.1)

In this case, $\Delta \overline{r^2}/a_0^2$ is computed from LU, DIU, LO, DIO (Function rrca). As before, the Stark broadening (due to collisions with electrons) is neglected ($C_4 = 0$). Radiative damping (γ_{rad}) is treated in the classical approximation.

In the case of a **single blended line** the 'line.dat' file looks as follows:

Example:

```
Mult
       namj
               ei
                       alam
                                 gflg
                                           dlgC6
                                                 lu diu
                                                           10
                                                                dio
                                                                      dlam
                                                                             ddlam
    3
O I ApJ Line 1: 67 6158.17 10.741 -1.140
    1 1 1
  67
       800
               10.741
                       6158.15
                                 -1.985
                                           1.0
               10.741
  67
       800
                       6158.17
                                 -1.140
                                           1.0
  67
       800
               10.741
                       6158.19
                                -0.553
                                                                      4.D-1
                                                                             4.D-3
         gfscale
clam
2000.0
```

Here kline = 1, ktotal = 3, nbl = 3, incode = [1, 1, 1]. Note that only the last of the rows describing the blend need entries C11 and C12.

As in the case of format '0', it is possible to enter an **equivalent width** $(W_0 \text{ in } [\text{mÅ}])$ in column C13. For this purpose, nbl must be negative, with |nbl| being the number of blend components. The gf value producing this equivalent width W_0 is returned in result.gflg01 (average 3D atmosphere) and result.gflg0x (1D reference atmosphere).

Example unblended line:

6.2 Line Data Formats 47

```
Mult
      namj ei
                    alam
                             gflg
                                    dlgC6 lu diu lo
                                                      dio dlam ddlam
 1 1
O I ApJ Line 2: 92
                    6300.30
                             0.000 - 9.773
-1 1
  92
       800
             0.000
                    6300.30
                            -9.773 1.0
                                          1
                                              0.0
                                                  2
                                                       0.0 4.D-1 4.D-3 7.00
clam
         qfscale
2000.0
         1.0
```

Example blended line:

```
dlgC6 lu diu lo
Mult
       nami
              ei
                    alam
                             gflg
                                                      dio dlam ddlam W0
 1 3
O I ApJ Line 1: 67
                    6158.17 10.741 -1.140
-3 1 1 1
  67
       800
            10.741
                    6158.15
                             -1.985 1.0
                                               0.0
                                                    2
                                                        0.0
                                           1
  67
       800
            10.741
                    6158.17
                             -1.140 1.0
                                          1
                                               0.0
                                                   2
                                                        0.0
  67
       800 10.741
                    6158.19 -0.553 1.0
                                          1
                                               0.0
                                                   2
                                                        0.0
                                                            4.D-1 4.D-3 10.00
         gfscale
clam
2000.0
         1.0
```

6.2.4 Single line calculations, complete line data format '2'

For a **single unblended line**, the this form of the 'line.dat' file looks like this.

Example:

```
Mult
                                                                   dlggr Crad dlam
                                      dlgC6 drrca1 dlgC4 C4lg
                                                                                       ddlam
                      alam
                               gflg
       nami
              ei
    1
Si I AA Line 5: 16
                     5948.540
                               5.0823
                                       -1.130
                                               390.03
                                                         11.80
   2
   16
       1400
              5.0823
                      5948.540 -1.130 1.0
                                             390.03 0.0
                                                            11.80
                                                                   0.0
                                                                          -1.0 5.D-1 5.D-3
clam
         gfscale
2000.0
         1.0
```

Description of entries:

```
Row 1: Header (identifies the meaning of the columns for data in row 5)
```

Row 2: Two integers, kline and ktotal

kline: number of line calculations requested in this file

ktotal: is the total number of spectral lines including blends

in this case kline = 1, ktotal = 1

Row 3: String, identifier of the (first) line calculation

Row 4: Integer *nbl*, integer array *incode*(*nbl*)

nb: number of blend components for this line calculation (= 1)

incode: integer array identifying the input format for each of the blend components (= 2)

Row 5: Line data in format '2' (11 + 2 columns):

- C1: Multiplet number (for information only)
- C2: Identifier of atom or ion (e.g. 2601 mean FeII)
- C3: Excitation potential of lower level in [eV]
- C4: Central wavelength of blend component
- C5: $\log qf$ value of blend component
- C6: $\Delta \log C_6$: Enhancement factor for van der Waals line broadening
- C7: $\Delta r^2/a_0^2$: Difference of mean square electron orbital radii
- C8: $\Delta \log C_4$: Enhancement factor for Stark line broadening
- C9: $-\log C_4$: Stark broadening constant.

```
if -\log C_4 = 0, then use Griem (Phys. Rev. 165, 258, 1968) and Cowley (Obs. 91, 139, 1971) approximation if -\log C_4 < 0 (typically -\log C_4 = -1.0), then C_4 = 0 C10: \Delta \log \gamma_{\rm rad}: Enhancement factor for natural line broadening C11: C_{\rm rad}: Natural line broadening (10^{-8}\gamma_{\rm rad}) if C_{\rm rad} < 0, use classical formula (\gamma_{\rm rad} = 2.22 \cdot 10^{15}/\lambda^2) [rad/s], where \lambda is in Å. C12: \Delta \lambda [Å]: Line profile is computed from \lambda_0 - \Delta \lambda to \lambda_0 + \Delta \lambda C13: \delta \lambda [Å]: Spacing of wavelength points for spectrum synthesis (C14: W_0 [mÅ]: total equivalent width of this blend, see below) Row 6: Description for data in row 6 Row 7: clam and gfscale (see Sect.6.1)
```

In the case of a **single blended line** the 'line.dat' file looks as follows:

Example:

```
Mult
                                                                                         ddlam
       nami
              ei
                       alam
                                gflg
                                       dlgC6 drrca1 dlgC4 C4lg
                                                                     dlggr Crad
                                                                                 dlam
Si I / Si II blend: 16
                          5948.540 5.0823 -1.130
                                                     390.03
    2 2
                       5948.540 -1.130
      1400
                                        1.0
                                               390.03
                                                       0.0
                                                             11.80
                                                                    0.0
                                                                            -1.0
   16
              5.0823
                                                                                 5.D-1 5.D-3
                      5948.530 -3.130
                                                90.00
                                                             13.80
                                                                            -1.0
   16
       1401
              0.0823
                                        1.0
                                                                    0.0
         gfscale
2000.0
```

Here kline = 1, ktotal = 2, nbl = 2, incode = [2, 2, 2]. Note that only the last of the rows describing the blend need entries C12 and C13.

As in the cases of format '0' and '1', it is possible to enter an **equivalent width** $(W_0 \text{ in } [\text{mÅ}])$ in column C14. For this purpose, nbl must be negative, with |nbl| being the number of blend components. The gf value producing this equivalent width W_0 is returned in result.gflg01 (average 3D atmosphere) and result.gflg0x (1D reference atmosphere). No examples are given since the necessary modification the data format should be obvious.

6.2.5 Single line calculations, complete line data format '3'

This data format has a maximum of 17 columns. It differs from format '2' only in the way the van der Waals broadening parameters are specified. Columns C7 with $\Delta \overline{r^2}/a_0^2$ is replaced by the four columns:

```
C7: LU: Orbital quantum number of valence electron of lower level C8: DIU: excitation energy [eV] of parent term for lower level C9: LO: Orbital quantum number of valence electron of upper level C10: DIO: excitation energy [eV] of parent term for upper level
```

as in format '1'. The remaining columns are as in format '2', but shifted by +3:

```
C11: \Delta \log C_4: Enhancement factor for Stark line broadening C12: -\log C_4: Stark broadening constant. if \log C_4 = 0, then use Griem (Phys. Rev. 165, 258, 1968) and Cowley (Obs. 91, 139, 1971) approximation if -\log C_4 < 0 (typically -\log C_4 = -1.0), then C_4 = 0 C13: \Delta \log \gamma_{\rm rad}: Enhancement factor for natural line broadening C14: C_{\rm rad}: Natural line broadening (10^{-8}\gamma_{\rm rad}) if C_{\rm rad} < 0, use classical formula (\gamma_{\rm rad} = 2.22 \cdot 10^{15}/\lambda^2) [rad/s], where \lambda is in Å.
```

6.2 Line Data Formats 49

```
C15: \Delta\lambda [Å]: Line profile is computed from \lambda_0 - \Delta\lambda to \lambda_0 + \Delta\lambda C16: \delta\lambda [Å]: Spacing of wavelength points for spectrum synthesis (C17: W_0 [mÅ]: total equivalent width of this blend, see below)
```

As in the cases of format '0', '1', and '2' it is also possible to enter an **equivalent width** (W_0 in [mÅ]), now in column C17. For this purpose, nbl must be negative, with |nbl| being the number of blend components. The gf value producing this equivalent width W_0 is returned in result.gflg01 (average 3D atmosphere) and result.gflg0x (1D reference atmosphere).

6.2.6 Single line calculations, complete line data format '4'

This data format has a maximum of 14 columns. It differs from format '2' only in the way the van der Waals broadening parameter is specified. Column C7 with $\Delta \overline{r^2}/a_0^2$ is replaced by the parameter – $\log C_6$.

C7: $-\log C_6$: negative logarithmic van der Waals broadening parameter C_6

The remaining columns are as in format '2'.

```
C8: \Delta \log C_4: Enhancement factor for Stark line broadening C9: -\log C_4: Stark broadening constant. if \log C_4 = 0, then use Griem (Phys. Rev. 165, 258, 1968) and Cowley (Obs. 91, 139, 1971) approximation if -\log C_4 < 0 (typically -\log C_4 = -1.0), then C_4 = 0 (no Stark broadening) C10: \Delta \log \gamma_{\rm rad}: Enhancement factor for natural line broadening C11: C_{\rm rad}: Natural line broadening (10^{-8}\gamma_{\rm rad}) if C_{\rm rad} < 0, use classical formula (\gamma_{\rm rad} = 2.22 \cdot 10^{15}/\lambda^2) [rad/s], where \lambda is in Å. C12: \Delta \lambda [Å]: Line profile is computed from \lambda_0 - \Delta \lambda to \lambda_0 + \Delta \lambda C13: \delta \lambda [Å]: Spacing of wavelength points for spectrum synthesis (C14: W_0 [mÅ]: total equivalent width of this blend, see above)
```

Example:

6707.840

5.0119

```
ei
                                     gflg
                                               dlgC6 C6log
                                                                 dlgC4 C4log
                                                                                  dlggr Crad dlam
                                                                                                        ddlan
Mult
       namj
                        alam
1 12
Li7, 6 components Li6, 6 components: glog=-0.427905 .. -0.831310
12 4 4 4 4 4 4 4 4 4 4 4 4
9999
       0300.7
                       6707.7560
                                                       31.3843
                                                                 0.0
                0.00
                                    -0.427905
                                               0.84
                                                                        14.1505
                                                                                  0.0
                                                                                         -1.0
       0300.7
                                    -0.206158
                                                       31.3843
                                                                                         -1.0
9999
                0.00
                       6707.7680
                                               0.84
                                                                 0.0
                                                                        14.1505
                                                                                  0.0
9999
       0300.7
                0.00
                        6707.9070
                                    -0.808148
                                               0.84
                                                       31.3844
                                                                 0.0
                                                                        14.1505
                                                                                  0.0
                                                                                         -1.0
9999
       0300.7
                0.00
                       6707.9080
                                    -1.507150
                                               0.84
                                                       31.3844
                                                                 0.0
                                                                        14.1505
                                                                                  0.0
                                                                                         -1.0
                       6707.9190
9999
       0300.7
                0.00
                                   -0.808148
                                               0.84
                                                       31.3844
                                                                 0.0
                                                                        14.1505
                                                                                  0.0
                                                                                         -1.0
       0300.7
                       6707.9200
                                   -0.808148
                                                       31.3844
9999
                0.00
                                               0.84
                                                                 0.0
                                                                        14.1505
                                                                                  0.0
                                                                                         -1.0
9999
       0300.6
                0.00
                        6707.9200
                                   -0.478953
                                               0.84
                                                       31.3844
                                                                 0.0
                                                                        14.1505
                                                                                         -1.0
                                                                                  0.0
9999
       0300.6
                0.00
                        6707.9230
                                   -0.178176
                                               0.84
                                                       31.3844
                                                                 0.0
                                                                        14.1505
                                                                                  0.0
                                                                                         -1.0
9999
       0300.6
                0.00
                       6708.0690
                                   -0.831310
                                               0.84
                                                       31.3844
                                                                 0.0
                                                                        14.1505
                                                                                  0.0
                                                                                         -1.0
9999
       0300.6
                0.00
                        6708.0700
                                    -1.734310
                                               0.84
                                                       31.3844
                                                                 0.0
                                                                        14.1505
                                                                                  0.0
                                                                                         -1.0
9999
                        6708.0740
                                                       31.3844
                                                                                         -1.0
       0300.6
                0.00
                                    -0.734310
                                               0.84
                                                                 0.0
                                                                        14.1505
                                                                                  0.0
9999
       0300.6
                        6708.0750
                                   -0.831310
                                               0.84
                                                       31.3844
                                                                 0.0
                                                                        14.1505
                                                                                  0.0
                                                                                         -1.0
                                                                                               10.D-1 5.D-3
               0.00
clam
         gfscale
```

6.2.7 Single line calculations, complete line data format '5'

This data format has a maximum of 15 columns. It differs substantially form format '4': (i) an extra column is inserted that allows the specification of $\log gf$ offsets; (ii) the van der Waals broadening is specified by $\log \gamma_6$ instead of $-\log C_6$; (iii) the Stark broadening is specified by $\log \gamma_4$ instead of $-\log C_4$; (iv) the natural broadening is specified by $\log \gamma_{\rm rad}$ instead of $\gamma_{\rm rad}/10^8$. More precisely, column C5-C15 have the following meaning in format '5':

C5: $\Delta \log gf$: Correction factor for the line's $\log gf$ value

C6: $\log gf$: the line's logarithmic gf value

C7: $\Delta \log \gamma_6$: Enhancement factor for van der Waals γ parameter

C8: $\log \left(\frac{\gamma_6 (T=10^4)}{N_{\rm H}} \right)$: logarithmic van der Waals broadening parameter $\gamma_6/N_{\rm H}$ at $T=10^4$ K.

C9: $\Delta \log \gamma_4$: Enhancement factor for Stark γ parameter

C10: $\log \left(\frac{\gamma_4 (T=10^4)}{N_e} \right)$: logarithmic Stark broadening parameter γ_4/N_e at $T=10^4$ K. if $\log \gamma_4/N_e \ge 0$, then use Griem (Phys. Rev. 165, 258, 1968) and Cowley (Obs. 91, 139, 1971) approximation

C11: $\Delta \log \gamma_{\rm rad}$: Enhancement factor for the natural line broadening

C12: $\log \gamma_{\text{rad}}$: Natural line broadening ($\log \gamma_{\text{rad}}$ [rad/s])

if $\log \gamma_{\rm rad} \ge 99.0$, use classical formula $(\gamma_{\rm rad} = 2.22 \cdot 10^{15}/\lambda^2)$ [rad/s], where λ is in Å.

C13: $\Delta\lambda$ [Å]: Line profile is computed from $\lambda_0 - \Delta\lambda$ to $\lambda_0 + \Delta\lambda$

C14: $\delta\lambda$ [Å]: Spacing of wavelength points for spectrum synthesis

(C15: W_0 [mÅ]: total equivalent width of this blend, see above)

Example:

```
Mult
               ei
                      alam
                                 dlggf gflg
                                                  dlgg6
                                                          g6log
                                                                  dlgg4
                                                                          g4log
                                                                                   dlggr grlog dlam
                                                                                                       ddlam
1 12
Li7, 6 components Li6, 6 components: glog=-0.427905 .. -0.831310
12 5 5 5 5 5 5 5 5 5 5 5 5
                                0.00 -0.427905 2.10 -7.94973
                                                                                   0.0
9999
       0300.7 0.00
                      6707.7560
                                                                  0.00
                                                                         -5.7800
                                                                                         99.0
                                                                                         99.0
9999
       0300.7
               0.00
                      6707.7680
                                0.00 -0.206158
                                                  2.10
                                                       -7.94974
                                                                  0.00
                                                                         -5.7800
                                                                                   0.0
9999
       0300.7
                      6707.9070
                                                  2.10
                                                       -7.94975
                                                                                   0.0
                                                                                         99.0
               0.00
                                0.00 - 0.808148
                                                                  0.00
                                                                         -5.7800
9999
       0300.7
               0.00
                      6707.9080
                                0.00 - 1.507150
                                                  2.10
                                                       -7.94975
                                                                  0.00
                                                                         -5.7800
                                                                                   0.0
                                                                                         99.0
9999
       0300.7
               0.00
                      6707.9190
                                0.00 - 0.808148
                                                 2.10
                                                       -7.94975
                                                                  0.00
                                                                         -5.7800
                                                                                   0.0
                                                                                         99.0
9999
       0300.7
               0.00
                      6707.9200
                                0.00 - 0.808148
                                                 2.10
                                                       -7.94975
                                                                  0.00
                                                                         -5.7800
                                                                                   0.0
                                                                                         99.0
9999
       0300.6
               0.00
                      6707.9200
                                 0.00
                                      -0.478953
                                                  2.10
                                                       -7.94975
                                                                  0.00
                                                                         -5.7800
                                                                                   0.0
                                                                                         99.0
9999
       0300.6 0.00
                      6707.9230 0.00 -0.178176 2.10
                                                       -7.94975
                                                                  0.00
                                                                         -5.7800
                                                                                   0.0
                                                                                         99.0
                                                                                   0.0
                                                                                         99.0
9999
       0300.6 0.00
                      6708.0690 0.00 -0.831310 2.10 -7.94976
                                                                  0.00
                                                                         -5.7800
9999
       0300.6 0.00
                      6708.0700 0.00 -1.734310 2.10 -7.94976
                                                                  0.00
                                                                         -5.7800
                                                                                   0.0
                                                                                         99.0
9999
       0300.6 0.00
                      6708.0740 0.00
                                      -0.734310 2.10
                                                       -7.94976
                                                                  0.00
                                                                         -5.7800
                                                                                   0.0
                                                                                         99.0
                      6708.0750 0.00
                                                                                         99.0 10.D-1 5.D-3
       0300.6 0.00
                                      -0.831310 2.10
                                                       -7.94976
                                                                  0.00
                                                                         -5.7800
                                                                                   0.0
9999
        gfscale
clam
6707.840 5.0119
```

6.2.8 Single line calculations, complete line data format '6'

This data format also has a maximum of 15 columns. It differs from format '5' only in the way the van der Waals broadening parameters are specified. In format '6', column C7–C8 have the following meaning:

C7: σ_{ABO} : van der Waals broadening cross section in atomic units at $v_0 = 10$ km/s according ABO theory C8: α_{ABO} : α parameter of ABO theory defining the velocity (temperature) dependence of the cross section σ .

The remaining columns C9-C15 are as in format '5'. Note that:

• no enhancement factor for van der Waals broadening is foreseen in this line data format.

6.2 Line Data Formats 51

• the temperature dependence of the broadening cross section is correctly taken into account according to the ABO theory when this line data format is used.

Example:

```
Mult
                                                                                          dlggr grlog dlam
                                                                                                                ddlam
       namj
                       alam
                                  dlggf gflg
                                                    s_abo
                                                               a abo
                                                                        dlgg4
                                                                                 g4log
1 12
Li7, 6 components Li6, 6 components: glog=-0.427905 .. -0.831310
12 6 6 6 6 6 6 6 6 6 6 6
                                                                                                 99.0
9999
       0300.7 0.00
                       6707.7560
                                  0.00
                                       -0.427905
                                                    355.909
                                                               0.40000
                                                                        0.00
                                                                                -5.7800
                                                                                          0.0
                                                    355.900
                                                                                                99.0
9999
       0300.7
               0.00
                       6707.7680
                                  0.00
                                        -0.206158
                                                               0.40000
                                                                        0.00
                                                                                -5.7800
                                                                                          0.0
       0300.7
               0.00
                       6707.9070
                                  0.00
                                        -0.808148
                                                    355.892
                                                               0.40000
                                                                                -5.7800
                                                                                                99.0
9999
                                                                        0.00
                                                                                          0.0
       0300.7
               0.00
                       6707.9080
                                  0.00
                                         -1.507150
                                                    355.892
                                                               0.40000
                                                                                                99.0
9999
                                                                        0.00
                                                                                -5.7800
                                                                                          0.0
9999
       0300.7
               0.00
                       6707.9190
                                  0.00
                                         -0.808148
                                                    355.892
                                                               0.40000
                                                                                -5.7800
                                                                                                99.0
                                                                        0.00
                                                                                          0.0
9999
       0300.7
               0.00
                       6707.9200
                                  0.00
                                         -0.808148
                                                    355.892
                                                               0.40000
                                                                        0.00
                                                                                -5.7800
                                                                                          0.0
                                                                                                 99.0
9999
       0300.6
               0.00
                       6707.9200
                                  0.00
                                         -0.478953
                                                    355.892
                                                               0.40000
                                                                        0.00
                                                                                -5.7800
                                                                                          0.0
                                                                                                 99.0
9999
       0300.6
               0.00
                       6707.9230
                                  0.00
                                         -0.178176
                                                    355.892
                                                               0.40000
                                                                        0.00
                                                                                -5.7800
                                                                                          0.0
                                                                                                 99.0
9999
       0300.6
               0.00
                       6708.0690
                                  0.00
                                         -0.831310
                                                    355.894
                                                               0.40000
                                                                        0.00
                                                                                -5.7800
                                                                                          0.0
                                                                                                 99.0
9999
       0300.6
               0.00
                       6708.0700
                                  0.00
                                         -1.734310
                                                    355.894
                                                               0.40000
                                                                        0.00
                                                                                -5.7800
                                                                                          0.0
                                                                                                 99.0
9999
       0300.6
               0.00
                       6708.0740
                                  0.00
                                         -0.734310
                                                    355.894
                                                               0.40000
                                                                        0.00
                                                                                -5.7800
                                                                                          0.0
                                                                                                 99.0
                                                                                                       10.D-1 5.D-3
                       6708.0750
                                        -0.831310
                                                               0.40000
                                                                                -5.7800
                                                                                                99.0
9999
       0300.6
               0.00
                                  0.00
                                                    355.894
                                                                        0.00
                                                                                          0.0
clam
         gfscale
6707.840 5.0119
```

6.2.9 Single line calculations, complete line data format '7'

This data format was designed for simple test calculations where the line profile is fixed, i.e. the line parameters are depth-independent (see also Sect. 3.5). This format has a maximum of 7 columns:

Description of entries:

C6: $\delta\lambda$ [Å]: Spacing of wavelength points for spectrum synthesis (C7: W_0 [mÅ]: total equivalent width of this blend, see above)

Row 6: Description for data in row 6

Row 7: clam and gfscale (see Sect.6.1)

Example:

```
alam  Vdop  eta0  avgt  dlam  ddlam
1  1
Test   grey sf  Vdop=2.D-5, eta0=1.0D0, avgt=1.D-2
1  7
```

```
4000.000 2.0D-5 1.0D0 1.0D-2 0.90D0 0.90D-2 clam gfscale -4000.000 1.0
```

6.2.10 Multiple Line Calculations

It is also possible to process a whole set of lines in a single run. The requirement is, however, that all lines have the same central wavelength (continuum wavelength). This mode was designed for parameter studies, e.g. investigating the "granulation abundance corrections" as a function of line excitation potential.

Example, 8 unblended N I lines of different excitation potential:

```
Mult
                                                drrca1 dlam
                                                                  ddlam
                                                                              W0
       namj chik
                      alam
                                gflg
                                         dlgC6
  8
    8
  N I Fictitious Line 1: /
                               0.000
                                        5500.0
                                                -7.6914
                                                          1.00
                                                                 10.00
                                                                         75.00 /
 -1
9999
             0.000
                      5500.0
                              -7.6914
                                        1.00
                                               10.00 3.00E-01
                                                                 3.00E-03
       700
                                                                             75.00
  N I Fictitious Line
                        2: /
                               2.000
                                        5500.0
                                                -5.7282
                                                                 10.00
                                                         1.00
                                                                         75.00 /
 -1
9999
       700
             2.000
                      5500.0
                              -5.7282
                                        1.00
                                               10.00
                                                      3.00E-01
                                                                 3.00E-03
                                                                             75.00
                               4.000
                                        5500.0
                                                -3.8298
                                                                 10.00
                                                                         75.00 /
  N I Fictitious Line
                        3: /
                                                         1.00
 -1
9999
       700
             4.000
                      5500.0
                              -3.8298
                                        1.00
                                               10.00 3.00E-01
                                                                 3.00E-03
                                                                             75.00
  N I Fictitious Line 4: /
                               6.000
                                        5500.0
                                                -1.9876
                                                                 10.00
                                                                         75.00 /
                                                         1.00
 -1
9999
       700
             6.000
                      5500.0
                              -1.9876
                                        1.00
                                               10.00 3.00E-01
                                                                 3.00E-03
                                                                             75.00
  N I Fictitious Line
                               8.000
                                        5500.0
                                                -0.1961
                                                                 10.00
                        5: /
                                                         1.00
                                                                         75.00 /
 -1
9999
       700
             8.000
                      5500.0
                              -0.1961
                                        1.00
                                               10.00 3.00E-01
                                                                 3.00E-03
                                                                             75.00
  N I Fictitious Line
                        6: /
                              10.000
                                        5500.0
                                                 1.5485
                                                         1.00
                                                                 10.00
                                                                         75.00 /
 -1
9999
       700 10.000
                      5500.0
                               1.5485
                                        1.00
                                               10.00
                                                       3.00E-01
                                                                 3.00E-03
                                                                             75.00
                              11.000
  N I Fictitious Line
                        7: /
                                        5500.0
                                                 2.4046
                                                         1.00
                                                                 10.00
                                                                         75.00 /
 -1
9999
       700 11.000
                      5500.0
                               2.4046
                                        1.00
                                                       3.00E-01
                                                                             75.00
                                               10.00
                                                                 3.00E-03
                              12.000
                                        5500.0
                                                 3.2510
                                                                         75.00 /
  N I Fictitious Line 8: /
                                                         1.00
                                                                 10.00
 -1
9999
       700
           12.000
                      5500.0
                               3.2510
                                       1.00
                                               10.00 3.00E-01
                                                                 3.00E-03
                                                                             75.00
         gfscale
clam
2000.0
         1.0
```

Note that now kline = 8, and ktotal = 8, since all lines have one blend component only.

6.3 Conversion of line broadening parameters

The line broadening can be specified in different ways, e.g. as $-\log C_4$ for quadratic Stark broadening. The required data is, however, not always available and must be converted from other broadening parameters, e.g. γ_4 . In the particular case of the *Vienna Atomic Line Database* the broadening is provided as $\log(\gamma_4/N_e)$ for a temperature of $T = 10^4$ K.

Please note that here and in Linfor3D in general, the parameters C_n (n = 4, 6) are defined via

$$\Delta\omega = \frac{C_n}{r^n} \tag{79}$$

whereas the definition by Unsöld is

$$\Delta\omega = 2\pi \frac{C_n}{r^n}. (80)$$

The Linfor parameters C_n are thus a factor 2π larger than in the definition by Unsöld.

Note that γ_{rad} , γ_4 , γ_6 measure the **full** width at half maximum of the Lorentzian profile in units of rad/s.

6.3.1 Quadratic Stark effect

The broadening parameter γ_4 for the quadratic Stark effect can be written as

$$\gamma_4 = 11.37 C_4^{2/3} v_{\text{rel}}^{1/3} N_e ,$$
 (81)

where $v_{\rm rel}$ is the relative velocity between the regarded atom and the perturber, i.e. the colliding particle:

$$v_{\rm rel}^2 = \frac{8 k T}{\pi m_{\rm H}} \cdot (\frac{1}{A_1} + \frac{1}{A_2}) \ .$$
 (82)

 A_1 and A_2 are the atomic weights in atomic mass units, e.g., $A_2 = 1$ for a colliding hydrogen atom and $A_1 \approx 56$ for iron atoms and $A_2 = 1/1837 = m_e/m_H$ for electrons. For Stark broadening with electrons as perturbers the following good approximation can be made:

$$A_1 >> A_2 \Rightarrow \frac{1}{A_1} + \frac{1}{A_2} \approx \frac{1}{A_2} = 1837 = m_{\rm H}/m_{\rm e}$$
 (83)

With this Eq. 81 can be written as

$$\log \frac{\gamma_4}{N_e} = \log 11.37 + \log C_4^{2/3} + \log v_{\text{rel}}^{1/3}$$
 (84)

$$= 1.056 + \frac{2}{3}\log C_4 + \frac{1}{6}\log \frac{8kT}{\pi m_e}$$
 (85)

$$= 1.056 + \frac{2}{3}\log C_4 + 1.931 + \frac{1}{6}\log T \tag{86}$$

$$= 1.056 + \frac{2}{3}\log C_4 + 1.931 + \frac{1}{6}\log 10^4 + \frac{1}{6}\log \frac{T}{10^4 \,\mathrm{K}}$$
 (87)

(88)

With $T = 10^4$ K, which is assumed for data in VALD, we derive

$$\log \frac{\gamma_4}{N_e} = 3.654 + \frac{2}{3} \log C_4 \tag{89}$$

and finally the conversion formula:

$$\log C_4 = 1.5 \log \frac{\gamma_4}{N_e} - 5.4805 \tag{90}$$

For instance a value of -5.491 from VALD gives $\log C_4 = -13.717$. The parameter C41g is thus set to 13.717.

6.3.2 Van der Waals broadening

The broadening parameter γ_6 for the van der Waals effect can be written as

$$\gamma_6 = 8.08 C_6^{2/5} v_{\text{rel}}^{3/5} N_{\text{H}} . \tag{91}$$

The perturbing particles are mostly hydrogen atoms with $A_2 = 1$. We now make the approximation

$$A_1 > A_2 \Rightarrow \frac{1}{A_1} + \frac{1}{A_2} \approx \frac{1}{A_2} = 1$$
 (92)

With this the relative velocity of the particles (Eq. 82) reduces to

$$v_{\rm rel}^2 = \frac{8 k T}{\pi m_{\rm H}}. (93)$$

We can thus rewrite Eq. 91:

$$\log \frac{\gamma_6}{N_{\rm H}} = \log 8.08 + \log C_6^{2/5} + \log v_{\rm rel}^{3/5} \tag{94}$$

$$= 0.907 + \frac{2}{5}\log C_6 + \frac{3}{10}\log \frac{8kT}{\pi m_{\rm H}}$$
 (95)

$$= 0.907 + \frac{2}{5}\log C_6 + 2.497 + \frac{3}{10}\log T \tag{96}$$

$$= 0.907 + \frac{2}{5}\log C_6 + 2.497 + \frac{3}{10}\log 10^4 + \frac{3}{10}\log \frac{T}{10^4 \,\mathrm{K}}$$
 (97)

(98)

With $T = 10^4$ K, which is assumed for data in VALD, we derive

$$\log \frac{\gamma_6}{N_{\rm H}} = 4.604 + \frac{2}{5} \log C_6 \tag{99}$$

and finally the conversion formula:

$$\log C_6 = 2.5 \log \frac{\gamma_6}{N_{\rm H}} - 11.510 \tag{100}$$

For instance a value of -7.619 from VALD gives $\log C_6 = -30.558$. Before LINFOR3D Version 6.5.0, neither the parameter γ_6 nor the parameter C6log= $-\log C_6$ could be specified in the line data file directly. Instead the van der Waals broadening had to be specified via the difference of mean square electron orbital radii $\Delta r^2/a_0^2$, where a_0 is the Bohr radius:

$$\log\left(\Delta \overline{r^2}/a_0^2\right) = \log C_6 + 32.3867 \ . \tag{101}$$

The necessary relation for the conversion between $(\Delta \overline{r^2}/a_0^2)$ and γ_6 is:

$$\Delta \overline{r^2}/a_0^2 = 10^{20.877 + 2.5 \log \frac{\gamma_6}{N_{\rm H}}} \ . \tag{102}$$

The exemplary value of -7.619 from VALD thus gives 67.437 for the parameter drrca1. In addition dlgC6 should be set to 0 unless you want to apply an additional enhancement of the broadening.

Since LINFOR3D Version 6.5.0, line data format '4' and '5' allows to enter directly the parameter C6log or γ_6/N_H , respectively.

6.3.3 ABO van der Waals broadening formalism

In the van der Waals broadening formalism of Anstee, Barklem, and O'Mara, γ_6 is computed as

$$\frac{w}{N_{\rm H}} = \frac{\gamma_6}{2 N_{\rm H}} = \sigma_{\rm ABO} a_0^2 \left(\frac{4}{\pi}\right)^{\alpha_{\rm ABO}/2} \Gamma(2 - \alpha_{\rm ABO}/2) v_0 \left(\frac{v_{\rm rel}}{v_0}\right)^{1 - \alpha_{\rm ABO}} , \tag{103}$$

where w is the **half** half width in rad s⁻¹, σ_{ABO} and α_{ABO} are the two tabulated quantities of the ABO line broadening theory, Γ denotes the mathematical Γ -function. The parameter σ_{ABO} is the broadening cross section at relative velocity $v_0 = 10 \, \text{km/s}$ between the perturbing hydrogen atom and the atom of interest in atomic units. The factor a_0^2 (a_0 is the Bohr radius) converts the cross section to units of cm². v_{rel} is the mean relative velocity averaged over the Maxwellian velocity distribution as given by Eq. 82.

The parameter α_{ABO} describes the velocity dependence of the broadening cross section

$$\sigma_{\text{ABO}}(v) = \sigma_{\text{ABO}}(v_0) \left(\frac{v}{v_0}\right)^{-\alpha_{\text{ABO}}}$$
 (104)

For details see, e.g., Barklem, Anstee and O'Mara, Publ. Astron. Soc. Aust., 1998, 15, 3368. Numerically, we obtain

$$\log \frac{\gamma_6}{N_{\rm H}} = \log \sigma_{\rm ABO} + 0.052455\alpha_{\rm ABO} + \log \Gamma (2 - \alpha_{\rm ABO}/2) + (1 - \alpha_{\rm ABO}) \log \left(\frac{v_{\rm rel}}{v_0}\right) - 10.25177. \quad (105)$$

This relation may be compared to the classical van der Waals formula (Eq.94) which may be rewritten as

$$\log \frac{\gamma_6}{N_{\rm H}} = 0.4 \log C_6 + 0.6 \log \left(\frac{v_{\rm rel}}{v_0}\right) + 4.5074114. \tag{106}$$

We can convert the ABO parameters σ_{ABO} and α_{ABO} to C_6 by requiring the two expressions (105) and (106) to yield identical results for $\gamma_6(v_{\rm rel} = v_0) = \gamma_6(T \approx 4760 \, {\rm K})$:

$$\log C_6 = 2.5 \log \sigma_{ABO} + 0.1311376 \alpha_{ABO} + 2.5 \log \Gamma (2 - \alpha_{ABO}/2) - 36.89795. \tag{107}$$

For $\sigma_{ABO} = 530$, $\alpha_{ABO} = 0.277$, we obtain $\log C_6 = -30.1076$.

If we choose a different reference velocity, v^* , for matching both expressions, we obtain

$$\log C_6 = 2.5 \log \sigma_{ABO} + 0.1311376 \alpha_{ABO} + 2.5 \log \Gamma (2 - \alpha_{ABO}/2) + \left(1 - \frac{5}{2} \alpha_{ABO}\right) \log \frac{v^*}{v_0} - 36.89795.$$
(108)

This relation shows that, for $\alpha_{ABO}=2/5$, ABO and LINFOR3D can be matched to give identical γ_6 for arbitrary temperatures. In LINFOR3D we choose $v^*=14.495$ km/s, corresponding to $T\approx 10^4$ K. Then $\log(v^*/v_0)=0.1612$.

On the other hand, any C_6 can be uniquely converted to σ_{ABO} and α_{ABO} :

$$\log \sigma_{ABO} = 0.4 \log C_6 + 14.76906834$$
 , $\alpha_{ABO} = 2/5$. (109)

For example, $\log C_6 = -30.1076$ implies $\log \sigma_{ABO} = 2.7260324$ or $\sigma_{ABO} = 532.15$.

For use in LINFOR3D, we rewrite Eq. (105) as

$$\log \frac{\gamma_6}{10^8} = \log \sigma_{ABO} + \frac{1 + \alpha_{ABO}}{2} \log \theta + \log P_{H} + F(\alpha_{ABO}), \qquad (110)$$

where $\theta = 5039.67/T$, $P_{\rm H} = N_{\rm H} k T$ is the partial pressure of neutral hydogen atoms, and

$$F(\alpha_{ABO}) = c_1 \alpha_{ABO} + \log \Gamma (2 - \alpha_{ABO}/2) - (1 - \alpha_{ABO}) \log v_0 + \frac{1 - \alpha_{ABO}}{2} c_2 - \frac{1 + \alpha_{ABO}}{2} c_3 + c_4,$$
(111)

or

$$F(\alpha_{ABO}) = \log \Gamma (2 - \alpha_{ABO}/2) + f_1 \alpha_{ABO} + f_2, \qquad (112)$$

with the constants

$$v_0 = 10^6 \,[\text{cm/s}], \tag{113}$$

$$a_0 = 5.2917725 \, 10^{-09}$$
, Bohr radius [cm], (114)

$$c_1 = \frac{1}{2} \log \left(\frac{4}{\pi} \right) = 0.052455,$$
 (115)

$$c_2 = \log\left(\frac{8}{\pi m_{\rm H}}\right) = 24.182288\,,$$
 (116)

$$c_3 = \log(k5039.67) = -12.15750,$$
 (117)

$$c_4 = \log\left(\frac{2v_0 a_0^2}{10^8}\right) = -18.25177,$$
 (118)

$$f_1 = c_1 - (c_2 + c_3)/2 + \log(v_0) = 0.040060295,$$
 (119)

$$f_2 = (c_2 - c_3)/2 + c_4 - \log(v_0) = -6.0818740$$
. (120)

For $\alpha_{ABO} = 2/5$ we obtain

$$\log \frac{\gamma_6}{10^8} = \log \sigma_{ABO} + \frac{7}{10} \log \theta + \log P_{H} - 6.0967212, \tag{121}$$

and with Eq. (109) we get

$$\log \frac{\gamma_6}{10^8} = \frac{2}{5} \log C_6 + \frac{7}{10} \log \theta + \log P_{\rm H} + 8.6723475, \tag{122}$$

which is the standard formula used in LINFOR3D for decades.

6.3.4 Natural line broadening

The broadening parameter γ_{rad} can be converted like this:

$$C_{\rm rad} = 10^{\log \gamma_{\rm rad} - 8.0} \tag{123}$$

For instance, $\log \gamma_{\rm rad} = 7.877$ would give $C_{\rm rad} = 0.753$. In line data formats '0' - '4', the parameter Crad is thus set to 0.753, and dlggr is set to 0.0. In line data formats '5' - '6', the parameter grlog is set to 7.887.

7.1 uio_save 57

7 Output files

LINFOR3D generates the following output files in the LINFOR3Dworking directory:

name		content
linfor_3D_1.uiosave	:	UIO formatted structures:
		ABU, ATOM, CMD, CONST, INFO, LINE (see Sect. 8.1 for de-
		tails).
linfor_3D_2.uiosave	:	UIO formatted structures:
		CONTF, IMUPHI, MAPS, RESULT (see Sect. 8.2 for details).
linfor_3D_3.uiosave	:	UIO formatted structure:
		CONTF3D – written to file if cc3d flag is set to 1 in CMD (see
		Sect. 8.3 for details).
linfor_1X.uiosave	:	UIO formatted structures:
		ABU, ATOM, CMD, CONST, INFO, LINE, CONTF, IMUPHI,
		RESULT – writen to file if run flag is set to –3 in CMD (See
		Sect. 8.4 for details).
linfor_timing.txt	:	Timing statistics (see Sect. 11).
linfor_3D_1.ps	:	Postscript file: local line profiles plus average.
linfor_3D_2.ps	:	Postscript file: line profiles for 1D reference atmospheres and
		time-averaged 1D and 3D spectra; granulation abundance correc-
		tion
<pre><lhd_model_name>_150.3x3</lhd_model_name></pre>	:	The 1D LHD model written as a 3X3 RHD box in UIO format
<3D_model_name>_avg.3x3	:	The $\langle 3D \rangle$ model written as a 3X3 RHD box in UIO format

The latest versions of Linfor3D (version 6.0.0 onwards) are compatible with the CVS versions of GNU data language (GDL)¹. To make this possible, two new routines were written to replace the intrinsic IDL I/O routines, SAVE/RESTORE, previously used by Linfor3D. Both these new routines, written by A. J. Gallagher, were written to exploit the Universal Input Output (UIO) routines, which were designed by B. Freytag for handling I/O in CO⁵BOLD.

7.1 uio_save

The uio_save.pro routine is rather complex, but is nevertheless designed to work as a viable replacement to the intrinsic IDL routine, SAVE. Therefore its call is simple. At the current time, the maximum number of variables uio_save can save is 15. This can be extended when necessary by adding further variables into the routine, but for the purposes of Linfor3D it was not required.

It saves a binary file, which is commonly given the file format name uiosave. A typical call for this routine is as follows:

```
uio_save, FILE = '<filename>', variable1, variable2, variableN [, /verbose]
```

where <filename> is a string of the exact file name to be used; variable1 - variableN are the variable names to be saved.

The uio_save.pro routine can save scalars, arrays and structures. However, at present, the UIO routines do not work with IDL pointers.

The switch verbose can be used to output several useful checks to screen, including the results of an error check, which is performed by the UIO routines throughout the save procedure. This is particularly

¹The tarball can be downloaded at http://gnudatalanguage.cvs.sourceforge.net/ and the GDL manual can be found at http://gnudatalanguage.sourceforge.net

58 7 OUTPUT FILES

useful for error checking one's own coding. As a simple example, the uio_save routine is used to save a scaler, two arrays and a structure and then uio_restore (see Sect. 7.2) is used to open the saved file below:

```
IDL> a = 45L \& b = findgen(100) \& c = dblarr(50, 100, /nozero)
IDL> d = \{a:a, b:b, c:c\}
IDL> uio_save, FILE = 'example.uiosave', a, b, c, d, /verbose
% UIO_SAVE: Writing A vector to file
% UIO_SAVE: Write of A successful
% UIO_SAVE: Writing B vector to file
% UIO_SAVE: Write of B successful
% UIO_SAVE: Writing C vector to file
% UIO_SAVE: Write of C successful
% UIO_SAVE: Writing D structure to file
% UIO_SAVE: Write of D successful
% UIO_SAVE: Closing file and checking...
% UIO_SAVE: Data has been successfully written to file
% UIO_SAVE: Write status: done
IDL> .reset ; reset the session and delete variable(s)
IDL> uio_restore, 'example.uiosave', /verbose
% UIO_RESTORE: Restoring structure A
% UIO_RESTORE: Restoring structure B
% UIO_RESTORE: Restoring structure C
% UIO_RESTORE: Restoring structure D
IDL> help
% At $MAIN$
              LONG
                                 45
В
              FLOAT
                      = Array[100]
C
              DOUBLE = Array[50, 100]
D
              STRUCT
                      = -> <Anonymous> Array[1]
```

The routine calls upon the following sub-routines from the UIO database directly:

Routine		Description
uio_filedefinc.pro	:	Parameter definitions for standard file descriptors and labels
uio_uionaminc.pro	:	Common block that contains parameters for UIO initialisation routines
uio_init.pro	:	Initialisation procedure for UIO routine package.
uio_wr.pro	:	Writes scalar or array data to file.
uio_wrlabl.pro	:	Writes a label for structures or datasets.
uio_openwr.pro	:	Opens a file for writing and writes the data block header.
uio_closwr.pro	:	Closes a file after writing.

Each of these sub-routines call on several other sub-routines within the UIO routine package.

A very simple example of how to use these sub-routines to write a basic structure to file in IDL or GDL (without using uio_save.pro) is given with step-by-step annotations:

Create a structure, C, with arrays A and B:

```
IDL> a = findgen(100) & b = fltarr(20, 50) & c = {a:a, b:b}
Initialise the UIO procedures and common blocks:
IDL> @uio_filedefinc
IDL> @uio_uionaminc
IDL> uio_init, progrm = 'example_save'
```

7.1 uio_save 59

Open a binary file (form = 'unformatted') called test.uiosave and use the default conversion type (conv = 'ieee_4'):

```
IDL> uio_openwr, nc, 'test.uiosave', outstr, ierr, $
IDL> form = 'unformatted', conv = 'ieee_4', prog = 'example_save'
```

Write the name of the dataset to file for the binary file header using special definition dataset_ident:

```
IDL> uio_wrlabl, nc, dataset_ident, outstr, ierr, date = 'now', $
IDL> name = 'test.uiosave'
```

Write the structure name, C, to file using special definition box_ident:

```
IDL> uio_wrlabl, nc, box_ident, outstr, ierr, date = 'now', name = 'c'
```

Begin the write of the C structure to file by declaring the box ID name as C using special definition box_id_ident:

```
IDL> uio_wr, nc, 'C', box_id_ident, name = 'C structure'
```

Write the contents of structure C to file:

```
IDL> uio_wr, nc, c.a, 'A', outstr, ierr, name = 'c.A'
IDL> uio_wr, nc, c.b, 'B', outstr, ierr, name = 'c.B'
```

Declare the end of the structure write using special definition endbox_ident:

```
IDL> uio_wrlabl, nc, endbox_ident, outstr, ierr
```

Declare the end of the dataset write using special definition enddataset_ident:

```
IDL> uio_wrlabl, nc, enddataset_ident, outstr, ierr
```

Close the file for writing

```
IDL> uio_closwr, nc, outstr, ierr
```

The uio_save.pro routine and other sub-routines within the Linfor3D routine list use this basic principle to write structures to file. A similar (though not as complex) set of procedures are used when writing arrays or scalars to file:

Create two arrays, A and B, and a scalar, C:

```
IDL> a = findgen(100) \& b = fltarr(20, 50) \& c = 55L
```

Initialise the UIO procedures and common blocks:

```
IDL> @uio_filedefinc
IDL> @uio_uionaminc
IDL> uio_init, progrm = 'example_save'
```

Open a binary file (form = 'unformatted') called test.uiosave and use the default conversion type (conv = 'ieee_4'):

```
IDL> uio_openwr, nc, 'test.uiosave', outstr, ierr, $
IDL> form = 'unformatted', conv = 'ieee_4', prog = 'example_save'
```

Write the name of the dataset to file for the binary file header using special definition dataset_ident:

```
IDL> uio_wrlabl, nc, dataset_ident, outstr, ierr, date = 'now', $
IDL> name = 'test.uiosave'
```

Write the arrays/scalars to file:

```
IDL> uio_wr, nc, a, 'A', outstr, ierr, name = 'A'
IDL> uio_wr, nc, b, 'B', outstr, ierr, name = 'B'
IDL> uio_wr, nc, c, 'C', outstr, ierr, name = 'C'
```

60 7 OUTPUT FILES

Declare the end of the dataset write using special definition enddataset_ident:

```
IDL> uio_wrlabl, nc, enddataset_ident, outstr, ierr
Close the file for writing
IDL> uio_closwr, nc, outstr, ierr
```

7.2 uio_restore

The uio_restore.pro routine is a wrapper designed around the high level IDL function uio_dataset_rd.pro to read a UIO formatted binary or ASCII file and return the output to the call level within IDL or GDL. The call procedure for this wrapper is identical to that of the intrinsic RESTORE procedure in IDL, i.e.:

```
uio_restore, '<filename>' [, variable1, variable2, ..., variableN [, /verbose]] where variables 1—N are optional, but useful where computer memory is limited. An example of its use:
```

```
IDL> uio_restore, 'linfor_3D_1.uiosave', /verbose
% UIO_RESTORE: Restoring structure ABU
% UIO_RESTORE: Restoring structure ATOM
% UIO_RESTORE: Restoring structure CMD
% UIO_RESTORE: Restoring structure CONST
% UIO_RESTORE: Restoring structure LINE
% UIO_RESTORE: Restoring structure INFO
IDL> help
% At $MAIN$
ABU
              STRUCT
                      = -> <Anonymous> Array[1]
MOTA
             STRUCT
                      = -> <Anonymous> Array[1]
CMD
                      = -> <Anonymous> Array[1]
             STRUCT
                      = -> <Anonymous> Array[1]
CONST
             STRUCT
INFO
              STRUCT
                      = -> <Anonymous> Array[1]
                     = -> <Anonymous> Array[1]
LINE
              STRUCT
```

The user can specify what data should be restored by adding additional command(s) to the call:

Additionally, this routine will open all CO⁵BOLD model atmospheres and is useful when a single piece of information (e.g. the model time) is required. It also means that for the first time, the user has a choice of computer languages (FORTRAN/IDL/GDL) to do their analysis without the need for any conversion of the output file. Further details of the routine's use can be found in the header of uio_restore.pro, which is located in the Routines sub-directory of Linfor3D.

7.3 Useful UIO information

The UIO routines allow the user to restore arrays with up to four dimensions, as modifying the UIO routines for use with FORTRAN so that more than four dimensions can be read is not a trivial matter. In its current form, the UIO routines will successfully save an array with more than four dimensions:

```
IDL> a = fltarr(10, 10, 10, 10, 10, 10, /nozero)
IDL> uio_save, file = 'example.uiosave', a, /verbose
% UIO_SAVE: Writing A vector to file
% UIO_SAVE: Write of A successful
% UIO_SAVE: Closing file and checking...
% UIO_SAVE: Data has been successfully written to file
% UIO_SAVE: Write status: done
however, the routines will not allow you to open the file afterwards:
IDL> uio_restore, 'example.uiosave'
% Attempt to subscript SARR with NDIM is out of range.
% Execution halted at: UIO_ST2DIM
  /data/Linfor/uio/uio_st2dim.pro
%
                    UIO_RD
                                     140
  /data/Linfor/uio/uio_rd.pro
                    UIO_STRUCT_RD
%
                                    333
  /data/Linfor/uio/uio_struct_rd.pro
%
                    UIO_DATASET_RD 150
  /data/Linfor/uio/uio_dataset_rd.pro
%
                    UIO_RESTORE
  /data/Linfor/Linfor_6_0_2/Routines/uio_restore.pro
%
                    $MAIN$
```

It is shown that the restore procedure fails during the uio_st2dim.pro sub-routine call. If one only wishes to work in IDL or GDL, and has little interest in working under FORTRAN, there is a very simple modification that can be added to the UIO routines so that an array with more than four dimensions can be saved and successfully restored under the UIO convention. At line 69 in the routine uio_st2dim.pro, the following is seen sarr=strarr(2,4), where 4 represents the maximum number of dimensions that the UIO routines (in IDL and GDL) can load. The user can simply replace 4 with a higher number so that larger dimension arrays can be successfully restored using the UIO routines. However, it must be stressed that any alteration to this routine will only affect any file opened in IDL and GDL, not in FORTRAN. Indeed, any attempt to open these larger dimension arrays in FORTRAN will result in a read failure.

For further details on the UIO repository, as well as some other examples, please consult the CO⁵BOLD manual², (Sect. 4).

²Downloadable at http://www.astro.uu.se/~bf/co5bold_main.html.

8 Output file structures

The binary files saved by Linfor3D contain several structures. In this section, a brief description of each array in every output structure is given.

8.1 linfor_3D_1.uiosave

The UIO formatted output file linfor_3D_1.uiosave contains the following structures:

8.1.1 ABU

The ABU structure contains information on the input file, <ABUFILE>.abu, found in the Data sub-directory of Linfor3D, where <ABUFILE> is either kiel, cifist2006 or special. It is created after the successful initialisation of the routine ionopa.pro.

Description of entries:

NAMI : Column 1 from abuid.

ABUI : Column 2 from abuid.

NAMIX : Column 1 from abuidx (version 6.2.2 onwards). See Sect. 5.3

ABUIX : Column 2 from abuidx (version 6.2.2 onwards). See Sect. 5.3

8.1.2 ATOM

The ATOM structure contains information on the input file, atom.dat, found in the Data sub-directory of LINFOR3D, e.g. 1201.24 corresponds to Mg II 24, 1201.25 corresponds to Mg II 25, etc.

Description of entries:

NIONS: Number of species included in atom.dat
 ANAM: LINFOR3D formatted atoms, ions and molecules. (Column 1 of atom.dat)
 WTJ: Corresponding baryon masses of ANAM. (Column 2 of atom.dat)
 CHIJ: Corresponding χ (eV) energies of ANAM (Column 3 of atom.dat)
 FISO: Corresponding isotope fractions of ANAM. Usually = 1.0, unless the isotopes are considered. (Column 4 of atom.dat)

This file can be edited before running LINFOR3D to alter, for example, isotope fractions. However 'line.dat' should be properly formatted to reflect the changes.

8.1.3 CMD

This structure contains inputs defined by the user in the linfor_setcmd.pro routine (plus additional parameters defined by linfor_checkcmd.pro). See Sect. 5 for details.

This input structure routine can be defined and compiled in IDL/GDL before running LINFOR3D by writing a BASH/TCSH script to produce this file using the native EOS procedure. This is usually done to run LINFOR3D when several sessions need to be computed at the same time.

8.1.4 **CONST**

This structure contains a set of constants used by Linfor3D throughout the synthesis.

8.1 linfor_3D_1.uiosave 63

Description of entries:

AVMEOS : Average mass of heavy particles in EOS.

AVMION : Average mass of heavy particles in IONDIS of the model.

EPSHE : Helium number density of the model. FRACH : Hydrogen mass fraction of the model.

AVMIONX : Average mass of heavy particles in IONDIS of the spectrum.

EPSHEX : Helium number density of the spectrum. FRACHX : Hydrogen mass fraction of the spectrum.

LUTAU1 : Smallest $\log \tau_{ROSS}$ covered by sub-model (refined z-grid) – set by user in

linfor_setcmd.pro

LUTAU2 : Largest $\log \tau_{ROSS}$ covered by sub-model (refined z-grid) – set by user in

linfor_setcmd.pro

LUTAU : Array of $\log \tau_{ROSS}$ values covered by sub-model (refined z-grid) UTAU : Array of τ_{ROSS} values covered by sub-model (refined z-grid)

NUTAU : Number of points in LUTAU

LCTAU1 : Smallest $\log \tau_0$ used for RT integration – set by user in linfor_setcmd.pro LCTAU2 : Largest $\log \tau_0$ used for RT integration – set by user in linfor_setcmd.pro

LCTAU : Array of $\log \tau_0$ points used for the RT integration CTAU : Array of τ_0 points used for the RT integration

NCTAU : Number of points in LCTAU

ICG : Index number of points over which the Curve-of-Growth is computed. Default:

51. Can be set in CMD structure by user.

DLGF_CG : $\Delta \log qf$ index used to compute the Curve-of-Growth. By default this is set at 51

points between $-0.5 \le \Delta \log gf \le +1.0$, but the user can extend this if the CoG

control parameters are set in the CMD structure (see CMD.COG).

IMT : The index number of microturbulence values over which to compute the Curve-

of-Growth. If CMD.MICRO = 0 then IMT = 1.

XIMC_MTX : The range of microturbulence values over which to compute the Curve-of-Growth

using the 1D external atmosphere.

XIMC_MT1 : The range of microturbulence values over which to compute the Curve-of-Growth

using the average 3D atmosphere.

MLIST : String array of CO5BOLD full files used during the spectrum synthesis run.

NFILE : Number of model files for which the spectrum synthesis was done NDATA : Number of snapshots for which spectrum synthesis was done

WALFAO : Switch for the ALFA parameter, which is related to the upper boundary condition

(0/1). ALFA = $H_{\rm P_0}/H_{\tau_0}$ – 1, where $H_{\rm P_0}$ and H_{τ_0} is the pressure scale height and the optical depth scale height, respectively, at the upper boundary. If WALFA0 =

1, $H_{\tau_0} = f \times H_{P_0}$, where f is $-H_{\tau_0}$ (if $-10 < H_{\tau_0} < 0$).

WALFA1 : Switch for the ALFA parameter, which is related to the upper boundary condition

(0/1). ALFA = H_{P_0}/H_{τ_0} – 1, where H_{P_0} and H_{τ_0} is the pressure scale height and the optical depth scale height, respectively, at the upper boundary. If WALFA1 =

1, $H_{\tau_0} = f \times H_{P_0}$, where f is $-H_{\tau_0}$ (if $H_{\tau_0} > 0$).

WALFA2 : Switch for the ALFA parameter, which is related to the upper boundary condition

(0/1). ALFA = H_{P_0}/H_{τ_0} – 1, where H_{P_0} and H_{τ_0} is the pressure scale height and the optical depth scale height, respectively, at the upper boundary. If WALFA2 =

1, $H_{\tau_0} = f \times H_{P_0}$, where f is $-H_{\tau_0}$ (if $H_{\tau_0} \le -10$).

YR1 : Plot ranges used by linfor_plot0.pro.
YR2 : Plot ranges used by linfor_plot0.pro.
YR3 : Plot ranges used by linfor_plot0.pro.
YR4 : Plot ranges used by linfor_plot0.pro.
YR5 : Plot ranges used by linfor_plot0.pro.
YR6 : Plot ranges used by linfor_plot0.pro.

8.1.5 INFO

The INFO structure contains information about the machine that Linfor3D was run on.

Description of entries:

VERSION : Version of Linfor3D used for synthesis run

DATE : Date of synthesis run

MACHINE : Machine used for synthesis run (Sometimes missing from INFO structure)

8.1.6 LINE

The LINE structure contains wavelength information and line parameters on the synthesis. This structure is typically used to reconstruct the equivalent wavelength array for use with the RESULT and IMUPHI structures.

Description of entries:

KLINE : Number of line calculations done by the synthesisKTOTAL : Total number of spectral lines including blends

K1 : Array containing corresponding index numbers of each line or blend in kline

NBLEND : Array containing number of blends for each line synthesis

CLAM : Central wavelength, λ_0 , and continuum wavelength in Å, set in line file

DLAM : Line profile, $\Delta \lambda$, in Å computed from $\lambda_0 - \Delta \lambda$ to $\lambda_0 + \Delta \lambda$ DDLAM : Spacing of wavelength points for spectrum synthesis

WLAMO : Requested equivalent width from line file. (set to '0' unless user includes W0 in

line.dat, see Sect. 6.2.2).

LINEID : Header from the line file

LFLAG : Control string set to 'cont' (continuum synthesis) or 'line' (line synthesis) by con-

tents of line file.

MULT : Integer array identifying the multiplet number of the lines synthesised ANAM : The atomic number of lines included in the synthesis (multiplied by 100)

WTJ : Array of baryon masses for every transition considered during spectrum synthesis

(taken from atom.dat).

CHIJ : Array of χ values of lower energy in eV for every transition considered during

synthesis (taken from [cifist2006, special, kiel].abu input file).

FISO : Array of isotope fractions for every transition considered during spectrum synthe-

sis (taken from atom.dat).

CHIK Array containing χ values of upper energy in eV **ALAM** Central wavelength of line or blend component **GFLG** Array containing $\log gf$ values of lines synthesised Array containing $\log C_6$ values of lines synthesised C6LOG Array containing $\Delta \log C_6$ values of lines synthesised DLGC6 Difference of mean square electron orbital radii, $\Delta r^2/a_0^2$ DRRCA1 C4LOG Array containing $\log C_4$ values of lines synthesised Array containing $\Delta \log C_4$ values of lines synthesised DLGC4 Natural line broadening parameter, γ_{rad} of KLINE. GRAD8

DLGGR : Array of mean square electron orbital radii differences $(\Delta \overline{r^2}/a_0^2)$

VDOP : Doppler width in units of the speed of light.

8.2 linfor_3D_2.uiosave 65

ETA0 : $\eta_0 = \kappa_l/\kappa_c$. See Sect. 3.5 and Fig. 1 AVGT : Damping parameter "a" for Voigt profile.

ILOWER[,3,X] : Lower level index from NLTE departure files (XBC) IUPPER[,3,X] : Upper level index from NLTE departure files (XBC)

XBCFIL3 : String array containing XBC information for the 3D synthesis (set to "LTE" if no

XBC is used)

XBCFILX : String array containing XBC information for the 1D synthesis (set to "LTE" if no

XBC is used)

XCFLAG : Set to 'grey': Continuum source funtion was set to wavelength-integrated Planck-

Function, $S = \sigma T^4/\pi$ and continuum opacity is set to Rosseland mean opacity,

 $\kappa_0 = \kappa_{\text{ROSS}}$. Set to 'mono': spectrum synthesis was computed as normal.

8.2 linfor_3D_2.uiosave

The UIO formatted output file linfor_3D_2.uiosave contains the following:

8.2.1 **CONTF**

NZ3

The arrays found in this structure relate to the contribution functions calculated by Linfor3D. See Sect. 3.4 for the formal derivations.

Description of entries:

NZX : Array containing resultant sampling considered during external 1D model synthesis, redefined by lctau1 and lctau2 set in linfor_setcmd.pro
 ZZX : Vertical geometrical ray scale for the 1D external model.
 CCX : Continuum intensity contribution functions of the external 1D model for "vertical" rays on the geometrical scale, ZZX.
 NZ1 : Array containing resultant sampling considered during (3D) log τ_{ROSS} synthesis, redefined by lctau1 and lctau2 set in linfor_setcmd.pro
 ZZ1 : Vertical geometrical ray scale for the (3D) model.
 CC1 : Continuum intensity contribution functions of the (3D) model for "vertical" rays on

the geometrical scale, ZZ1.

Array containing resultant sampling considered during 3D synthesis, redefined by lctau1 and lctau2 set in linfor_setcmd.pro

ZZ3 : Vertical geometrical ray scale for the 3D model.

CC3 : Continuum intensity contribution functions of the 3D model for "vertical" rays on

the geometrical scale, ZZ3.

 $\begin{array}{lll} \text{LTAUC} & : & \text{Array of } \log \tau_0 \text{ (continuum optical depth) points} \\ \text{LTAURX} & : & \text{Array of } 1D \log \tau_{ROSS} \text{ (Rosseland optical depth) points} \\ \end{array}$

DTRTCX : $d \log \tau_{ROSS}/d \log \tau_0$ for the external 1D model used by linfor_cf2cr.pro.

LTAUR1 : Array of $\langle 3D \rangle \log \tau_{ROSS}$ points.

DTRTC1 : $d \log \tau_{ROSS} / d \log \tau_0$ for the $\langle 3D \rangle$ model used by linfor_cf2cr.pro.

LTAUR3 : Array of 3D $\log \tau_{ROSS}$ points

DTRTC3 : $d \log \tau_{ROSS}/d \log \tau_0$ for the 3D model used by linfor_cf2cr.pro.

CFCXI : Array containing the 1D Continuum Intensity Contribution Function, C_I^c , evaluated

over a $\log \tau_0$ scale

CFC1I : Array containing the $\langle 3D \rangle$ Continuum Intensity Contribution Function, C_I^c , evaluated

over a $\log \tau_0$ scale

CFC3I : Array containing the 3D Continuum Intensity Contribution Function, C_I^c , evaluated

over a $\log \tau_0$ scale, see Eq. (42).

CFLXI : Array containing the 1D *Line Intensity Contribution Function*, C_I^l , evaluated over a $\log \tau_0$ scale

CFL1I : Array containing the $\langle 3D \rangle$ *Line Intensity Contribution Function*, C_I^l , evaluated over a $\log \tau_0$ scale

CFL3I : Array containing the 3D *Line Intensity Contribution Function*, C_I^l , evaluated over a $\log \tau_0$ scale, see Eq. (46).

CFDXI : Array containing the 1D *Line Intensity Depression Contribution Function*, $\tilde{C}_I^D = C_I^c - C_I^l$, evaluated over a log τ_0 scale

CFD1I : Array containing the $\langle 3D \rangle$ Line Intensity Depression Contribution Function, $\tilde{C}_I^D = C_I^c - C_I^l$, evaluated over a $\log \tau_0$ scale

CFD3I : Array containing the 3D Line Intensity Depression Contribution Function, $\tilde{C}_I^D = C_I^c - C_I^l$, evaluated over a log τ_0 scale, see Eq. (50).

CFWXI : Array containing the 1D Equivalent Width Intensity Contribution Function, C_I^W , evaluated over a log τ_0 scale

CFW1I : Array containing the $\langle 3D \rangle$ Equivalent Width Intensity Contribution Function, C_I^W , evaluated over a log τ_0 scale

CFW3I : Array containing the 3D Equivalent Width Intensity Contribution Function, C_I^W , evaluated over a log τ_{cont} scale, see Eq. (56).

CFCXF : Array containing the 1D Continuum Flux Contribution Function, C_F^c , evaluated over a $\log \tau_0$ scale

CFC1F : Array containing the $\langle 3D \rangle$ Continuum Flux Contribution Function, C_F^c , evaluated over a $\log \tau_0$ scale

CFC3F : Array containing the 3D Continuum Flux Contribution Function, C_F^c , evaluated over a log τ_0 scale, see Eq. (44).

CFLXF : Array containing the 1D *Line Flux Contribution Function*, C_F^l , evaluated over a $\log \tau_0$ scale

CFL1F : Array containing the $\langle 3D \rangle$ *Line Flux Contribution Function*, C_F^l , evaluated over a $\log \tau_0$ scale

CFL3F : Array containing the 3D *Line Flux Contribution Function*, C_F^l , evaluated over a log τ_0 scale, see Eq. (48).

CFDXF : Array containing the 1D *Line Flux Depression Contribution Function*, C_F^D , evaluated over a log τ_0 scale

CFD1F : Array containing the $\langle 3D \rangle$ Line Flux Depression Contribution Function, C_F^D , evaluated over a $\log \tau_0$ scale

CFD3F : Array containing the 3D *Line Flux Depression Contribution Function*, C_F^D , evaluated over a log τ_0 scale, see Eq. (53).

CFWXF : Array containing the 1D Equivalent Width Flux Contribution Function, C_F^W , evaluated over a log τ_0 scale

CFW1F : Array containing the $\langle 3D \rangle$ Equivalent Width Flux Contribution Function, C_F^W , evaluated over a log τ_0 scale

CFW3F : Array containing the 3D Equivalent Width Flux Contribution Function, C_F^W , evaluated over a log τ_{cont} scale, see Eq. (59).

CRCXI : Array containing the 1D Continuum Intensity Contribution Function, C_I^c , evaluated over a $\log \tau_{\text{ROSS}}$ scale

CRC1I : Array containing the $\langle 3D \rangle$ Continuum Intensity Contribution Function, C_I^c , evaluated over a $\log \tau_{ROSS}$ scale

CRC3I : Array containing the 3D Continuum Intensity Contribution Function, C_I^c , evaluated over a log τ_{ROSS} scale, see Eq. (42).

CRLXI : Array containing the 1D *Line Intensity Contribution Function*, C_I^l , evaluated over a $\log \tau_{\rm ROSS}$ scale

CRL11 : Array containing the $\langle 3D \rangle$ *Line Intensity Contribution Function, C_I^l*, evaluated over a $\log \tau_{ROSS}$ scale

8.2 linfor_3D_2.uiosave 67

CRL3I : Array containing the 3D *Line Intensity Contribution Function*, C_I^l , evaluated over a $\log \tau_{\text{ROSS}}$ scale, see Eq. (46).

CRDXI : Array containing the 1D *Line Intensity Depression Contribution Function*, $\tilde{C}_I^D =$

 $C_I^c - C_I^l$, evaluated over a log τ_{ROSS} scale

CRD11 : Array containing the $\langle 3D \rangle$ Line Intensity Depression Contribution Function, $\tilde{C}_I^D = C_I^c - C_I^l$, evaluated over a log τ_{ROSS} scale

CRD3I : Array containing the 3D Line Intensity Depression Contribution Function, $\tilde{C}_I^D = C_I^c - C_I^l$, evaluated over a log τ_{ROSS} scale, see Eq. (50).

CRWXI : Array containing the 1D Equivalent Width Intensity Contribution Function, C_I^W , evaluated over a log τ_{ROSS} scale

CRW1I : Array containing the $\langle 3D \rangle$ Equivalent Width Intensity Contribution Function, C_I^W , evaluated over a log τ_{ROSS} scale

CRW3I : Array containing the 3D Equivalent Width Intensity Contribution Function, C_I^W , evaluated over a log τ_{ROSS} scale, see Eq. (56).

CRCXF : Array containing the 1D Continuum Flux Contribution Function, C_F^c , evaluated over a $\log \tau_{\text{ROSS}}$ scale

CRC1F : Array containing the $\langle 3D \rangle$ Continuum Flux Contribution Function, C_F^c , evaluated over a log τ_{ROSS} scale

CRC3F : Array containing the 3D Continuum Flux Contribution Function, C_F^c , evaluated over a log τ_{ROSS} scale, see Eq. (44).

CRLXF : Array containing the 1D $Line\ Flux\ Contribution\ Function,\ C_F^l,$ evaluated over a $\log au_{ROSS}$ scale

CRL1F : Array containing the $\langle 3D \rangle$ *Line Flux Contribution Function,* C_F^l , evaluated over a $\log \tau_{\rm ROSS}$ scale

CRL3F : Array containing the 3D *Line Flux Contribution Function*, C_F^l , evaluated over a $\log \tau_{\text{ROSS}}$ scale, see Eq. (48).

CRDXF : Array containing the 1D *Line Flux Depression Contribution Function*, C_F^D , evaluated over a log τ_{ROSS} scale

CRD1F : Array containing the $\langle 3D \rangle$ Line Flux Depression Contribution Function, C_F^D , evaluated over a log τ_{ROSS} scale

CRD3F : Array containing the 3D *Line Flux Depression Contribution Function*, C_F^D , evaluated over a log τ_{ROSS} scale, see Eq. (53).

CRWXF : Array containing the 1D Equivalent Width Flux Contribution Function, C_F^W , evaluated over a log τ_{ROSS} scale

CRW1F : Array containing the $\langle 3D \rangle$ Equivalent Width Flux Contribution Function, C_F^W , evaluated over a log τ_{ROSS} scale

CRW3F : Array containing the 3D Equivalent Width Flux Contribution Function, C_F^W , evaluated over a log τ_{ROSS} scale, see Eq. (59).

8.2.2 IMUPHI

This structure contains selective information from the RESULT structure (as well as information on ray angles). This structure is used in conjunction with several post-processing routines, such as linfor_rotate.pro.

Description of entries:

NDATA : Number of snapshots for which spectrum synthesis was done KLINE : Number of lines for which spectrum synthesis was done

NLAMX : Total number of wavelength and flux points in calculated in the synthesis

NMUPHI : Number of μ and ϕ angles used in the synthesis

MODELIDX	:	Name of the external 1D model atmosphere
MODELID3	:	String array containing the name of snapshot, the <i>x</i> and <i>y</i> sampling and snapshot
		time in seconds
MODELID1	:	String array containing the name of average model snapshot and snapshot time in seconds
DV3	:	Array containing a velocity-spaced wavelengths, $\left(\frac{\lambda-\lambda_0}{\lambda_0}\right)c_0$
MU	:	Array containing ray inclination angles, $\mu = \cos \theta$
PHI	:	Array containing azimuthal angles, ϕ
XMU	:	An extended array of inclination angles, conformal with NMUPHI dimension of other arrays – allows for a simple way to perform the flux integration; $\int I3\mu d\mu = \sum (I3 * XMU * WTS)$
ХРНІ	:	- ·
WTS	:	Weightings used for μ and ϕ angle quadratures
I1	:	Array of (3D) fluxes evaluated over NMUPHI angles: [NLAMX, NMUPHI, NDATA, KLINE]
D1	:	Array of (3D) line depression fluxes evaluated over NMUPHI angles: [NLAMX, NMUPHI, NDATA, KLINE]
13	:	Array of 3D fluxes evaluated over NMUPHI angles: [NLAMX, NMUPHI, NDATA, KLINE]
D3	:	
IX	:	

8.2.3 MAPS

DX

The output file linfor_3D_2.uiosave contains a structure MAPS. An example of this structure is:

NMUPHI, NDATA, KLINE]

Array of 1D line depression fluxes evaluated over NMUPHI angles: [NLAMX,

**	Structure	<83027f4>, 11 t	ags, length=11289820,	data	length=11289820,	refs=1:
	NX	LONG	140			
	NY	LONG	140			
	NDATA	INT	12			
	KLINE	INT	1			
	NLAM	LONG	11			
	MODELID	STRING	Array[12]			
	MU0	FLOAT	1.00000			
	PHI0	FLOAT	0.00000			
	CLAM	FLOAT	3966.34			
	LINEID	STRING	Array[1]			
	DV3	FLOAT	Array[11]			
	ICLAM0	FLOAT	Array[140, 140, 12]			
	ICLAM2	FLOAT	Array[140, 140, 11,	1, 12]	

Depending on the value of the control parameter $maps_flag$ (see Sect. 5.1), there might be a tag named ICLAM1

8.2 linfor_3D_2.uiosave 69

ICLAM1 FLOAT Array[140, 140, 12, 1]

instead of ICLAM2 or even both might be missing if $maps_flag = 0$.

Description of entries:

nx, ny : x,y dimensions of the 2D images

ndata : number of models for which spectrum synthesis was donekline : number of lines for which spectrum synthesis was done

clam : central continuum wavelength for all maps

modelid : model identifier (0:ndata-1)
lineid : line identifier (0:kline-1)

ICLAMO : continuum intensity maps for all models (at clam),

dimensions: nx, ny

(see Sect. 6)

ICLAM1 : emergent intensity maps for all models and lines,

including line absorption at clam (window center);

dimensions: nx, ny, ndata, kline; only present if maps_flag = 1

(see Sect. 6)

ICLAM2 : emergent intensity maps for all models and lines,

including line absorption at all wavelengths within the wavelength window

of width $2 \cdot dlam$ around the central wavelength clam:

 $\lambda_i = clam - dlam + i \cdot ddlam$, where clam = alam + dclam,

alam is the wavelength of the main blend component as defined in line.dat;

dimensions: nx, ny, nlam, kline, ndata;

only present if $maps_flag = 2$

(see Sect. 6)

W3LAM : equivalent width maps for all models and lines

Note:

- Intensities are given in units of $[erg cm^{-2} s^{-1} sr^{-1} Å^{-1}]$.
- The file formerly called "linfor_3D.idlsave" was renamed to "linfor_3D_1.idlsave".

Note that the maps include foreshortening effects. A model with a quadratic cross section becomes a rectangle when viewed off-center.

If ntheta≠ 0, the flux spectrum is computed as before, and the intensity maps show the vertical view, as before.

Keyword view added to plotting routine linfor_plot3. If given, the intensity and equivalent width maps show the foreshortened view.

8.2.4 RESULT

This structure contains all results from the radiative transfer done by Linfor3D, as well as some other useful information.

Description of entries:

NDATA : Number of snapshots for which spectrum synthesis was done
KLINE : Number of lines for which spectrum synthesis was done
KTOTAL : The total number of spectral lines including blends

NLAMX : Total number of wavelength and flux points in calculated in the synthesis

MU0 : Scalar containing first μ angle PHI0 : Scalar containing first ϕ angle

STRMU0 : String of MU0

MODELIDX : Name of the LHD model atmosphere

MODELID3 : String array containing the name of snapshot, the x and y sampling and snapshot

time in seconds

MODELID1 : String array containing the name of average model snapshot and snapshot time in

seconds

GRIDID : String array containing the sampling size of the synthesis

LINEID : String array containing the headers in the line file

LFLAG : Control string set to 'cont' (continuum synthesis) or 'line' (line synthesis) by con-

tents of line file.

VFACX : The x-component of the hydrodynamical velocity field of the 2D/3D models is

multiplied by this factor. Set in CMD.

VFACY : The y-component of the hydrodynamical velocity field of the 2D/3D models is

multiplied by this factor. Set in CMD.

VFACZ : The z-component of the hydrodynamical velocity field of the 2D/3D models is

multiplied by this factor. Set in CMD.

NL3 : Number of wavelength and flux points used for every line synthesised

DV3 : Array containing a velocity-spaced wavelengths

XIMICX : Array containing the microturbulences of the 1D synthesis
 XIMIC1 : Array containing the microturbulences of the ⟨3D⟩ synthesis
 XIMIC3 : Array containing the microturbulences of the 3D synthesis

GFLGOX : If the user sets an equivalent width 'WO' (stored in LINE.WLAMO) in the line file

(see Sects. 6.2.2 & 6.2.3) then this array will contain the resulting $\log gf$ value(s) necessary to compute the line or blend of that set strength from the given external

1D model atmosphere.

GFLG01 : If the user sets an equivalent width value in the line file (see Sects. 6.2.2 & 6.2.3)

then this array will contain the resulting $\log gf$ value(s) necessary to compute the

line or blend of that set strength from the $\langle 3D \rangle$ model atmosphere.

FX : Structure containing arrays of 1D fluxes fluxes (F) and intensities (I)

DX : Structure containing arrays of 1D line depression fluxes (F) and intensities (I) WX : Structure containing arrays of 1D equivalent widths for the absolute line depres-

sion (D) and intensity (I)

F1 : Structure containing arrays of (3D) fluxes fluxes (F) and intensities (I)

D1 : Structure containing arrays of ⟨3D⟩ line depression fluxes (F) and intensities (I)
 W1 : Structure containing arrays of ⟨3D⟩ equivalent widths for the absolute line depression

sion (D) and intensity (I)

F3 : Structure containing arrays of 3D fluxes fluxes (F) and intensities (I)

D3 : Structure containing arrays of 3D line depression fluxes (F) and intensities (I) W3 : Structure containing arrays of 3D equivalent widths for the absolute line depres-

sion (D) and intensity (I)

AC1 : Structure containing arrays of (3D) abundance corrections required to replicate

the equivalent 3D profiles for absolute line depression (D) and intensity (I)

ACX : Structure containing arrays of 1D abundance corrections required to replicate the

equivalent 3D profiles for absolute line depression (D) and intensity (I)

FCG1 : Contains the (3D) continuum intensity (I) and continuum flux (F). They are con-

stant, not changing with $\log gf$ or the line along the CoG.

WCG1 : Structure containing arrays of (3D) Curve-of-Growth equivalent width fluxes (F)

and intensities (I).

FCGX : Contains the external 1D continuum intensity (I) and continuum flux (F). They

are constant, not changing with $\log qf$ or the line along the CoG.

8.4 linfor_1X.uiosave 71

WCGX : Structure containing arrays of Curve-of-Growth equivalent width fluxes (F) and intensities (I) computed from the 1D external model atmospheres.

8.3 linfor_3D_3.uiosave

The UIO formatted output file linfor_3D_3.uiosave contains the following:

8.3.1 **CONTF3D**

The CONTF structure contains information relating to the 3D contribution functions. When the cc3d flag is set, this structure is saved and contains extended information from that stored in the CONTF structure.

Description of entries:

Description of entries.					
NX3	:	Resultant sampling points considered in synthesis, redefined by nx_skip set in			
		linfor_setcmd.pro			
NY3	:	Resultant sampling points considered in synthesis, redefined by ny_skip set in			
		linfor_setcmd.pro			
NZ3	:	Array containing resultant sampling considered during synthesis, redefined by lctau1			
		and lctau2 set in linfor_setcmd.pro			
ZZ3	:	Vertical geometrical ray scale for the 3D model.			
CC3	:	Continuum intensity contribution functions of the 3D model for "vertical" rays on the			
		geometrical scale, 773.			

8.4 linfor_1X.uiosave

This is a special output file, only written when Linfor3D performs synthesis under run_flag = -3. While most of the structures given in this file contain most of the same sub-structures and arrays that are found in linfor_3D_1.uiosave and linfor_3D_2.uiosave, the MAPS structure is not written and several sub-structures or arrays pertaining to the 3D or $\langle 3D \rangle$ synthesis. The only exception to this is the inclusion of the I3, D3, I1 and D1 arrays in the structure IMUPHI. This is so that certain post-synthesis routines, such as linfor_rotate.pro, still work without error. While these arrays exist, they only contain zeros.

72 9 PLOTTING OUTPUT

9 Plotting output

In this section we briefly present examples of how you can manipulate the output detailed in Sect. 8 and plot them in IDL or GDL.

9.1 Plotting the synthesis

Linfor3D has several routines that can quickly process the raw data from the uiosaves output after the synthesis has completed. The first of these is linfor_rotate.pro. The call procedure for this routine is:

```
A = linfor_rotate(IMUPHI, itime, kline, vsini [, /normalize, modid = modid])
```

where IMUPHI is the imuphi structure found in linfor_3D_2.uiosave; itime is the snapshot number (0-N-1) or the averaged time (-1); i_kline is the kline index; and vsini is the $v \sin i$ value of star in km s⁻¹. The switch, /normalize, is used to normalise the spectrum and keyword modid is used to select which synthesis to process $(1 = 1D, 2 = \langle 3D \rangle)$ and 3 = 3D.

The other useful routine is linfor_convol.pro. This routine is used to convolve a Gaussian profile with the synthesis. The call for this routine is:

```
linfor_convol, lambda, input_flux, output_flux, xi
```

where lambda is a 1D array containing the wavelength points; input_flux is a 1D array containing the corresponding unbroadened flux; output_flux is the 1D output array containing the broadened flux; and xi is a float/double scalar turbulence parameter in absolute units $-\xi = \sigma \sqrt{2} = \text{FWHM}/(\sigma \sqrt{2})$. Using both these routines will produce an array of flux points that can be plotted. The following step-by-step procedures can be used to successfully load and plot the synthesis.

After loading the two uiosaves, linfor_3D_1.uiosave and linfor_3D_2.uiosave, create a wavelength array for the number of lines synthesised (kline) and data points (nlamx):

```
IDL> lambda = fltarr(imuphi.nlamx, imuphi.kline)

IDL> for i = 0, imuphi.kline - 1 do begin &$

IDL> lambda[*, i] = (line.clam - line.dlam[i]) + $

IDL> findgen(1. + 2. * line.dlam[i] / line.ddlam[i]) * line.ddlam[i] &$

IDL> endfor

Create the corresponding flux arrays for the 3D, \langle 3D \rangle and 1D fluxes:

IDL> flux3 = fltarr(imuphi.nlamx, imuphi.kline) ; 3D flux array

IDL> flux1 = fltarr(imuphi.nlamx, imuphi.kline) ; <3D> flux array

IDL> fluxx = fltarr(imuphi.nlamx, imuphi.kline) ; 1D flux array

Set a v sin i value. For this example, we will set v sin i = 5 km/s:
```

```
IDL> vsini = 5.
```

```
Use the routine linfor_rotate.pro to produce the normalised flux for the 3D, (3D) (averaged over all
```

Use the routine linfor_rotate.pro to produce the normalised flux for the 3D, $\langle 3D \rangle$ (averaged over all snapshots):

```
IDL> for i = 0, imuphi.kline - 1 do begin &$
IDL> flux3[*, i] = linfor_rotate(imuphi, -1, i, vsini, /normalize, modid = 3) &$
IDL> flux1[*, i] = linfor_rotate(imuphi, -1, i, vsini, /normalize, modid = 2) &$
IDL> fluxx[*, i] = linfor_rotate(imuphi, -1, i, vsini, /normalize, modid = 1) &$
IDL> endfor
```

From this procedure, the 3D, $\langle 3D \rangle$ and 1D synthesis can be plotted in IDL or GDL using the plot command. However, if one wishes to include an instrumental broadening term in the synthesis, the

following demonstrates how to do this using the linfor_convol.pro.

Set up three new arrays for the convolved 3D, \langle 3D \rangle and 1D flux profiles:

```
IDL> f3_inst = make_array([size(flux3, /dimensions)])
IDL> f1_inst = make_array([size(flux1, /dimensions)])
IDL> fx_inst = make_array([size(fluxx, /dimensions)])
```

Set the instrumental broadening in km/s:

```
IDL> v inst = 10.0
```

and the speed of light in km/s:

```
IDL> c = 2.9979246D+5
```

Calculate the equivalent instrumental broadening value in absolute units:

```
IDL> inst = (v_inst * line.clam / c) / (2 * sqrt(alog(2)))
```

Using linfor_convol.pro to broaden flux3, flux1 and fluxx with a Gaussian of FWHM v_inst:

```
IDL> for i = 0, imuphi.kline - 1 do begin &$
IDL> linfor_convol, lambda[*, i], flux3[*, i], f3_inst[*, i], inst &$
IDL> linfor_convol, lambda[*, i], flux1[*, i], f1_inst[*, i], inst &$
IDL> linfor_convol, lambda[*, i], fluxx[*, i], fx_inst[*, i], inst &$
IDL> endfor
```

9.2 Plotting contribution functions

LINFOR3D also contains information on contribution functions. This section explains how to plot one type of contribution function, the equivalent width contribution functions (crw[3,1,X]f see Sect. 8.2.1), which are derived by integrating the line-depth contribution functions (Magain 1986, A&A, 135) over all wavelength points considered by LINFOR3D during the synthesis run. In this example, we will average over all snapshots computed during the synthesis as well. The crw[3,1,X]f has the following dimensions: [CONST.NCTAU, RESULT.NDATA, RESULT.KLINE]. Create the arrays and set some variables:

IDL> crw1f[*, j] = ln10 * avg(contf.crw1f[*, *, j], 1) * tauc / avg(f1[*, j]) &\$

```
IDL> crw3f = fltarr(const.nctau, result.kline)
IDL> crw1f = fltarr(const.nctau, result.kline)
IDL> crwxf = fltarr(const.nctau, result.kline)
IDL> f3 = fltarr(result.nlamx, result.kline)
IDL> f1 = fltarr(result.nlamx, result.kline)
IDL> fx = fltarr(result.nlamx, result.kline)
IDL> ltauc = contf.ltauc
IDL> tauc = 10.0^ltauc
IDL > ln10 = alog(10)
Fill the flux arrays:
IDL> for i = 0, result.kline - 1 do begin &$
IDL> f3[*, i] = avg(result.f3.f[*, *, i], 1) &
IDL> f1[*, i] = avg(result.f1.f[*, *, i], 1) &
IDL> fx[*, i] = result.fx.f[*, i] &
IDL> endfor
Convert the contribution functions from Eq. (59) to a \log \tau_{ROSS} scale:
IDL> for j = 0, result.kline - 1 do begin &$
IDL> crw3f[*, j] = ln10 * avg(contf.crw3f[*, *, j], 1) * tauc / avg(f3[*, j]) &$
```

74 9 PLOTTING OUTPUT

```
IDL> crwxf[*, j] = ln10 * avg(contf.crwxf[*, *, j], 1) * tauc / avg(fx[*, j]) &$ IDL> endfor
```

Finally, plot the contribution functions:

```
IDL> plot, ltauc,crwxf[*, 0], linestyle = 5
IDL> oplot, ltauc,crw3f[*, 0]
IDL> oplot, ltauc,crw1f[*, 0], linestyle = 4
```

The conversion just performed means that the plot depicts $dW/d \log \tau_{ROSS}$ (in mÅ) as a function of $\log \tau_{ROSS}$, where W is the equivalent width and $\log \tau_{ROSS}$ is the logarithm of the optical depth evaluated over a Rosseland scale. As such, $\int (dW/d \log \tau_{ROSS}) d \log \tau_{ROSS}$ reproduces the equivalent width in mÅ.

9.3 Plotting the Curve-of-Growth

The Curve-of-Growth (CoG) information is contained in three arrays within the RESULT, ABU and CONST structures CONST.dlgf_cg, RESULT.wcgx, RESULT.wcg1, ABU.abui and ABU.abuix, see Sect. 8 for information. The wcgx and wcg1 are four dimensional arrays formatted according to the number of snapshots considered during the spectrum synthesis, RESULT.ndata; the number of lines synthesised, RESULT/LINE.kline; the number of microturbulences to be evaluated, CONST.imt; and the number of index points to compute the CoG, CMD/CONST.icg.

To plot a traditional Curve-of-Growth (i.e. log(W) as a function of A(X)) the correct abundance should be known. This is usually given in ABU. abui (or ABU. abuix in version 6.2.2 onwards), if their corresponding abundance files are edited and input into LINFOR3D. Otherwise, this value should be input manually. In this example, we assume the former is accurate. First, let's define A(X), in this case we will work with lithium, A(Li):

```
IDL> N = 3
IDL> logA = abu.abui[N] + const.dlgf_cg
```

Next, let's define log(W), and average out the snapshot information:

```
IDL> logWX = fltarr(line.kline, const.imt, const.icg)
IDL> logW1 = fltarr(line.kline, const.imt, const.icg)
IDL> for k = 0, line.kline - 1 do begin &$
IDL> for i = 0, const.imt - 1 do begin &$
IDL> logWX[k, i, *] = alog10(avg(result.wcgx.f[*, k, i, *], 0)) &$
IDL> logW1[k, i, *] = alog10(avg(result.wcg1.f[*, k, i, *], 0)) &$
IDL> endfor &$
IDL> endfor
```

Finally, let's plot the first line for all microturbulence values:

```
IDL> plot, logA, logWX[0, 0, *]
IDL> for i = 1, const.imt - 1 do $
IDL> oplot, logA, logWX[0, i, *], linestyle = i
IDL> for i = 0, const.imt - 1 do $
IDL> oplot, logA, logW1[0, i, *], linestyle = i, color = 255
```

10 Installing GDL and running Linfor3D

While SourceForge© constantly update their libraries, to this date, the version of GDL supplied via their download libraries is not complete enough to successfully run Linfor3D. (This was last checked on 10/01/2017). Therefore, one needs to download the current CVS version of GDL.

LINFOR3D has only been successfully tested on CVS versions of GDL 0.9.4 and 0.9.5. We are currently testing LINFOR3D with GDL versions 0.9.6 and 0.9.7, however, so far we have been unsuccessful in getting LINFOR3D to run with them.

To install the CVS version of GDL after download ³ follow these basic instructions. Before installation, you will need to make sure that you have the latest version of cmake and eigan3 version 3.2.7 onwards (see GDL install notes⁴.

Once this is done, **as root**, create a directory in /usr/local called gdl and extract it to a named sub-directory of your choice. (This means that one can get later versions of GDL without deleting previous versions.) Finally make a sub-directory within that directory called build:

```
/ $> mkdir /usr/local/gdl
/ $> mkdir /usr/local/gdl/tarball
/ $> mv <gdl.tarball> /usr/local/gdl/tarball
/ $> cd /usr/local/gdl/
gdl/ $> tar -xzvf ../tarball/<gdl.tarball>
gdl/ $> cd gnudatalanguage
gnudatalanguage/ $> mkdir build
gnudatalanguage/ $> cd build
```

Run cmake within the build directory (if libraries are missing during the cmake procedure, install them as necessary and rerun cmake, making sure that you remove the CMakeCache.txt file beforehand). Then, once the procedure has successfully finished "make" the build (using all the computer cores, N, available):

```
build/ $> cmake ..
build/ $> make -j <N>
```

Once complete, add a symbolic link of the gdl command (<gdl_directory>/src/gdl) to /usr/local/bin/ and run gdl. To check the compatibility of the build, run the command "make check" from the build directory.

10.1 Running Linfor3D with GDL

Installing and running Linfor3D under GDL does not differ from running under IDL. However, for those who wish to exploit its new ability of running on GDL (e.g. use with HPC centres, etc.) a small change must be made in the routine monocubic.pro. Line 165 contains the following:

```
iout=(0 > long(interpol(findgen(n)+1.0,xin,xout))) < n</pre>
```

This must be replaced with the following more formal syntax, because of the minute differences in which GDL and IDL handle array information:

```
iout=(0 > long(interpol(findgen(n)+1.0,xin,[xout]))) < n</pre>
```

This change will not effect any part of the IDL version of Linfor3D, but prevents a fatal error when running Linfor3D under GDL.

Finally, copy your IDL_PATH and IDL_STARTUP to GDL_PATH and GDL_STARTUP, and add in the PRO library from the GDL install to the start of the GDL_PATH. If this is properly done, Linfor3D will run without error by using the start guide in Sect. 2.

³Available at http://gnudatalanguage.cvs.sourceforge.net/

⁴http://gnudatalanguage.sourceforge.net/

10.2 Running Linfor3D in parallel

The most important new feature of Linfor3D, now that it runs on GDL, is its ability to run in parallel without the concerns of IDL licenses. This means that completion times for jobs run sequentially can be split into much quicker jobs by, e.g. snapshot or wavelength interval (for large wavelength ranges), which can later be combined. Therefore, for the first time, one can compute large wavelength ranges or complex molecules in hours, not days or weeks. This requires you to create elaborate BASH or TCSH scripts that use EOFs to edit linfor_setcmd.pro.

11 Timing statistics

At the end of a run of LINFOR3D timing statistics are presented which are also saved to the file linfor_timing.txt in the current working directory. The file will look like this:

```
TIMING STATISTICS
_____
 Routine linfor_find_ff.....(total ): 10.36 s ( 0.00 %)
 Restoring structure FF.....
                                        ---
 5.17 s
                         (
                               1):
                                               (
                                                  0.00 %)
                                         5.57 s (
                         (
                               2) :
                                                  0.00 %)
                                                  0.00 %)
                         (
                               3):
                                        5.05 s (
                         (
                               4) :
                                        5.74 s (
                                                 0.00 %)
                         (
                               5):
                                        5.76 s ( 0.00 %)
                         (
                               6):
                                        4.87 s ( 0.00 %)
                               7):
                                        5.14 s (
                                                 0.00 %)
                         (
                               8):
                                         5.41 s (
                                                 0.00 %)
                         (
                         (
                               9):
                                         5.13 s (
                                                 0.00 %)
                              10):
                                        5.41 s (
                                                 0.00 %)
                         (
                                                 0.00 %)
                                        5.85 s (
                         (
                              11) :
                                        5.05 s (
                                                  0.00 %)
                         (
                              12) :
                                        4.76 s (
                                                  0.00 %)
                         (
                              13) :
                         (
                              14) :
                                        5.06 s (
                                                  0.00 %)
                              15) :
                                         4.74 s (
                                                  0.00 %)
                         (
                         (
                              16):
                                         4.72 s (
                                                  0.00 %)
                                         5.10 s (
                         (
                              17) :
                                                  0.00 %)
                                        4.93 s (
                                                  0.00 %)
                         (
                              18):
                                        4.91 s (
                              19) :
                                                 0.00 %)
 Routine linfor_ionopa_3d.....(total ):
                                      736.01 s (
                                                 0.12 %)
                                       36.80 s (
                         (average):
                                                 0.01 %)
                               0):
                                       38.12 s (
                                                 0.01 %)
                         (
                               1) :
                                        37.65 s (
                                                 0.01 %)
                         (
                         (
                               2):
                                        35.50 s (
                                                  0.01 %)
                                        40.03 s (
                         (
                               3):
                                                 0.01 %)
                                        38.03 s (
                         (
                               4) :
                                                 0.01 %)
                                        38.49 s (
                                                  0.01 %)
                         (
                               5):
                         (
                               6):
                                        37.90 s (
                                                  0.01 %)
                         (
                               7):
                                        36.29 s (
                                                  0.01 %)
                                        36.88 s (
                               8):
                         (
                                                  0.01 %)
                               9):
                                       37.29 s (
                                                  0.01 %)
                         (
                         (
                              10):
                                        37.04 s
                                               (
                                                  0.01 %)
                         (
                              11) :
                                        37.64 s (
                                                  0.01 %)
                              12) :
                                        36.05 s (
                                                  0.01 %)
                         (
                         (
                              13) :
                                       33.74 s (
                                                 0.01 %)
                                       35.52 s (
                                                 0.01 %)
                         (
                              14) :
                                        35.83 s (
                                                 0.01 %)
                         (
                              15):
                                        35.51 s (
                                                 0.01 %)
                              16):
                         (
                                        36.46 s (
                         (
                              17) :
                                                 0.01 %)
                                        36.14 s (
                                                  0.01 %)
                         (
                              18):
                              19) :
                                        35.90 s (
                         (
                                                  0.01 %)
 Saving structure FF.....
 Rad. transfer for 3D model....(total ): 594678.33 s ( 97.40 % )
                         (average): 29733.92 s ( 4.87 %)
                                     31170.96 s ( 5.11 %)
                         (
                               0):
```

78 11 TIMING STATISTICS

```
1):
                                               31021.06 s (
                                                              5.08 %)
                              (
                                      2):
                                               29445.84 s (
                                                              4.82 %)
                              (
                                      3):
                                               30393.73 s (
                                                              4.98 %)
                                      4):
                                               30423.26 s
                              (
                                                         (
                                                              4.98 %)
                              (
                                      5):
                                               29654.40 s
                                                          (
                                                              4.86 %)
                                                              4.77 %)
                              (
                                      6):
                                               29151.41 s
                                                          (
                                      7):
                                                              4.82 %)
                              (
                                               29403.00 s (
                                      8):
                                               29536.25 s
                                                              4.84 %)
                                                         (
                                      9):
                                               29749.70 s
                                                              4.87 %)
                              (
                                     10):
                                               33397.79 s
                                                              5.47 %)
                                                          (
                              (
                                     11):
                                               30029.57 s
                                                              4.92 %)
                                                          (
                              (
                                               29955.88 s
                                                              4.91 %)
                                     12) :
                                                          (
                              (
                                     13):
                                               28652.31 s
                                                              4.69 %)
                              (
                                     14):
                                               28731.89 s
                                                          (
                                                              4.71 %)
                                               29166.00 s (
                                                              4.78 %)
                              (
                                     15):
                                     16):
                                               28685.49 s (
                                                              4.70 %)
                                     17) :
                                               28832.02 s (
                                                              4.72 %)
                               (
                                     18):
                                               28688.46 s (
                                                              4.70 %)
                                     19):
                                               28589.31 s
                                                         (
                                                              4.68 %)
Rad. transfer for <3D> model....(total
                                       ) :
                                               14236.35 s
                                                          (
                                                              2.33 %)
                              (average):
                                                711.82 s
                                                              0.12 %)
                                                          (
                              (
                                      0):
                                                755.84 s
                                                          (
                                                              0.12 %)
                              (
                                                716.50 s
                                                              0.12 %)
                                      1) :
                                                          (
                              (
                                      2) :
                                                715.40 s
                                                              0.12 %)
                              (
                                                721.79 s
                                                              0.12 %)
                                      3):
                                                          (
                              (
                                      4):
                                                717.25 s
                                                              0.12 %)
                                                          (
                                                715.77 s
                              (
                                      5):
                                                              0.12 %)
                                                          (
                              (
                                      6):
                                                702.42 s
                                                          (
                                                              0.12 %)
                              (
                                      7):
                                                717.40 s
                                                          (
                                                              0.12 %)
                              (
                                      8):
                                                707.86 s (
                                                              0.12 %)
                                      9):
                                                703.97 s (
                                                              0.12 %)
                                     10):
                                                746.35 s (
                                                              0.12 %)
                               (
                                     11) :
                                                707.23 s (
                                                              0.12 %)
                                                695.03 s (
                               (
                                     12) :
                                                              0.11 %)
                                     13) :
                                                691.42 s
                                                              0.11 %)
                                                          (
                                     14) :
                                                690.57 s
                                                          (
                                                              0.11 %)
                               (
                                     15):
                                                736.33 s
                                                         (
                                                              0.12\%
                                     16):
                                                698.71 s (
                                                              0.11 %)
                                     17) :
                                                698.63 s
                                                         (
                                                              0.11 %)
                                     18) :
                                                701.31 s
                                                              0.11 %)
                                                          (
                              (
                                     19):
                                                696.56 s
                                                              0.11 %)
                                                          (
                                                              0.09 %)
Rad. transfer for 1D model....(total
                                                577.25 s
                                       ):
                                                          (
Total.....(total
                                       ) :
                                              610549.27 s ( 100.00 % )
```

The file is also saved during a running LINFOR3D process. Thus, time statistics are available even after aborting the process. The statistics show the system time needed for individual computation steps/routines of LINFOR3D and their contribution to the total time in percent. For the case that the same operation is performed several times, e.g., doing the radiative transfer for more than one model snap shot, the total of all calls, the average time, and the duration for each individual step is given (see example above).

12 IONDIS

IONDIS is responsible for computing all information on requested atomic and molecular species requested in the line.dat file. As stated in Sect. 2, IONDIS is run under FORTRAN. In this section, we will briefly outline the considerations made by IONDIS, and a full list of the limited number of atomic and molecular species IONDIS currently takes into account.

12.1 Atoms

LINFOR3D does not at present include the **complete** atomic data information used by CO⁵BOLD. Rather, a number of selected atoms are properly treated by IONDIS. Additions to IONDIS.f are welcome and will be integrated, after proper testing. However, we ask that **FULL** considerations are taken to the entire program flow of LINFOR3D before submitting them to us.

At present (version 6.2.5) there are 61 atomic species considered by IONDIS. You can change the atomic abundances considered during spectrum synthesis by changing the abuid (or abuidx in versions 6.2.2 onwards) and putting your changes in special.abu. Depending on how you want to run LINFOR3D (see Sect. 5.3), abuid and abuidx can be equal or different. If they are different, cifist2006.abu is treated as the model abundance file (and is loaded into abuid) and special.abu is treated as the spectrum abundance file (and is loaded into abuidx). A full list of the atoms (and ionisation states, isotopes) are given below.

Table 15: List of atomic species currently considered by IONDIS

Species	Considered	Considered
	ionisation states	isotopes
Н	I	
Не	I, II	
Li	I, II	6, 7
Be	I, II	
C	I, II	
N	I, II	
0	I, II	
F	I, II	
Ne	I, II	
Na	I, II	
Mg	I, II	24, 25, 26
Al	I, II	
Si	I, II	
P	I, II	
S	I, II	
Cl	I, II	35, 37
Ar	I, II	
K	I, II	
Ca	I, II	
Sc	I, II	
Ti	I, II	
V	I, II	
Cr	I, II	
Mn	I, II	
Fe	I, II	
Co	I, II	

80 12 IONDIS

Ni	I, II	l I
Cu	I, II	63, 65
Zn	I, II	05, 05
As	I, II I, II	···
Rb	I, II, III	···
Sr	I, II, III	
Y	I, II	
Zr	I, II	
Nb	I, II	
Mo	I, II	
Ru	I, II	
Rh	I, II	
Pd	I, II	
Ag	I, II	
Ba	I, II	134, 135, 136, 137, 138
La	I, II	
Ce	I, II	
Pr	I, II	
Nd	I, II	
Sm	I, II	
Eu	I, II	
Gd	I, II	152, 154, 155, 156, 157, 158, 160
Dy	I, II	
Er	I, II	162, 164, 166, 167, 168, 170
Tm	I, II	
Yb	I, II	168, 170, 171, 172, 173, 174, 176
Lu	I, II	175, 176
Hf	I, II	
Ta	I, II	
W	I, II	
Os	I, II	
Pb	I, II	
Th	I, II	
U	I, II	

12.2 Molecules

LINFOR3D also considers a *limited* number of molecules. At present they are only diatomic/bimetallic molecules. We welcome new integrations into IONDIS, and will include them into the general realise, after they are properly tested. However, we ask that **FULL** considerations are taken to the entire program flow of LINFOR3D before submitting them to us.

Table 16: Small molecular network: 5 atoms, 8 molecules

	Н	С	N	О	Mg
Н	H ₂	СН	NH	ОН	MgH
C	CH	C_2	CN	CO	_
N	NH	CN	_	_	_
О	OH	CO	_	_	_
Mg	MgH	_	_	_	

12.2 Molecules 81

	Н	Li	С	N	О	F	Mg	Ti	Cr	Fe
Н	H ₂	LiH	СН	NH	OH	FH	MgH		CrH	FeH
Li	LiH	_	_	_	LiO	_		_	_	
C	CH	_	C_2	CN	CO	_		_	_	
N	NH	_	CN	_	_	_		_	_	
О	OH	LiO	CO	_	_	_		TiO	_	
F	FH		_	_	_	_			_	
Mg	MgH	_	_	_	_	_		_	_	
Ti	_	_	_	_	TiO	_		_	_	
Cr	CrH	_	_	_	_	_		_	_	
Fe	FeH		_	_	_	_			_	

Table 17: Large molecular network: 10 atoms, 14 molecules

Some definitions 12.2.1

 N_i Total number density of nuclei of element i, including nuclei bound in diatomic molecules

 \tilde{N}_i Number density of nuclei of element i not bound in diatomic molecules

 $\tilde{N}_{i,0}$ Number density of neutral nuclei of element i not bound in diatomic molecules

Total number density of diatomic molecules made up of one $N_{i,k}$

nucleus of element i, and one nucleus of element k

 N_e Total electron number density.

 $N_{\text{Kern}} = \sum_{i} N_{i}$ Total number density of nuclei of all elements, diatomic molecules counting as 2 nuclei

 $P_e = N_e kT$ Electron pressure.

 $f_i = N_i/N_{\rm Kern}$ Fractional abundance of element i (constant) $x_i = \tilde{N}_i / N_{\text{Kern}}$

Fractional abundance of free nuclei of element i.

 $x_i = f_i = const.$ for elements not involved in molecule formation $(i \notin \{i_{mol}\})$. For elements forming molecules ($i \in \{i_{mol}\}$), x_i is the variable to be iterated.

 $x_{i,k} = N_{i,k}/N_{\text{Kern}}$ Fractional abundance of molecule (i, k).

 $x_e = N_e/N_{\rm Kern}$ Fractional abundance of free electrons (iterated quantity).

12.2.2 Equations

The Saha equation provides the relation between $\tilde{N}_{i,0}$ and \tilde{N}_{i} :

$$\tilde{N}_{i,0} = S_{i,0} \, \tilde{N}_i \tag{124}$$

where the Saha factor $S_{i,0}$ depends on temperature and electron pressure (and on the ionization potentials and the partition functions of the different ionization stages).

Molecule partial pressures are given by the relation

$$P_{i,k} = \frac{P_i P_k}{K_{i,k}} \tag{125}$$

where $K_{i,k}$ is the dissociation constant for the (neutral) diatomic molecule (ik), composed of one nucleus of elements i and k each. P_i and P_k are the partial pressures of the **neutral** atoms of elements i and k, respectively. Since P = N kT, molecule densities are

$$N_{i,k} = \frac{kT \, \tilde{N}_{i,0} \, \tilde{N}_{k,0}}{K_{i,k}} \tag{126}$$

82 12 IONDIS

Dividing by N_{Kern} , we obtain the fractional molecule abundance

$$x_{i,k} = \frac{N_{i,k}}{N_{\text{Kern}}} = \frac{N_{\text{Kern}} kT \ x_i S_{i,0} \ x_k S_{k,0}}{K_{i,k}} = \frac{P_e \ x_i S_{i,0} \ x_k S_{k,0}}{K_{i,k} \ x_e} = D_{i,k} \frac{x_i \ x_k}{x_e}$$
(127)

where we have defined

$$D_{i,k} = P_e \frac{S_{i,0} S_{k,0}}{K_{i,k}}. (128)$$

We note that $D_{i,k}$ depends only on T and P_e , but not on absolute number densities, and hence is constant during the iteration.

For all elements i involved in molecule formation, $i \in \{i_{mol}\}$, we have the following conservation equation

$$f_i = x_i + \sum_k x_{i,k} (1 + \delta_{i,k})$$
 (129)

or

$$x_i + \sum_{k} D_{i,k} \frac{x_i \ x_k}{x_e} (1 + \delta_{i,k}) = f_i$$
 (130)

where $\delta_{i,k}$ is the Kronecker symbol, accounting for the correct counting of atoms in molecules with two identical components.

The electron density is given by

$$N_e = \sum_{i} \tilde{N}_i \overline{Z}_i = \sum_{i \in \{i_{mol}\}} \tilde{N}_i \overline{Z}_i + \sum_{i \notin \{i_{mol}\}} \tilde{N}_i \overline{Z}_i$$
 (131)

where the mean degree of ionization of element i, \overline{Z}_i is defined as

$$\overline{Z}_{i} = \sum_{j=-1,3} j \, \tilde{N}_{i,j} / \sum_{j=-1,3} \tilde{N}_{i,j} = \frac{1}{\tilde{N}_{i}} \sum_{j=-1,3} j \, \tilde{N}_{i,j} = \sum_{j=-1,3} j \, \tilde{S}_{i,j} = \sum_{j=1,3} j \, \tilde{S}_{i,j} - \tilde{S}_{i,-1}.$$
 (132)

Here index j runs over the 4 ionization stages j = 0...3 of element i. For elements forming negative ions, the sum includes the negative ion, j = -1. For such elements, \overline{Z}_i may become negative! Note that \overline{Z}_i depends only on T and P_e , but not on the degree of molecule formation. Dividing Eq.(131) by N_{Kern} , we obtain

$$x_e = \sum_{i} x_i \overline{Z}_i = \sum_{i \in \{i, \dots, l\}} x_i \overline{Z}_i + \sum_{i \notin \{i, \dots, l\}} x_i \overline{Z}_i$$
(133)

Defining

$$f_e = \sum_{i \notin \{i_{mol}\}} x_i \, \overline{Z}_i = \sum_{i \notin \{i_{mol}\}} f_i \, \overline{Z}_i = const. \tag{134}$$

we have finally

$$x_e - \sum_{i \in \{i_{mol}\}} x_i \, \overline{Z}_i = f_e \tag{135}$$

Combining Eq.(130) and (135), we have the following vector equation

$$\vec{X} + \vec{F}(\vec{X}) = \vec{R} \tag{136}$$

where

$$\vec{X} = \{x_1, x_2, \dots x_N, x_e\},\tag{137}$$

is the vector of unknown number fractions, and

$$\vec{R} = \{f_1, f_2, \dots f_N, f_e\} = const.,$$
 (138)

is the known (constant) right-hand side. N is the number of chemical elements included in the molecular network. Equation (136) is a system of N+1 nonlinear algebraic equations which can be solved for \vec{X} by Newton-Raphson iteration.

12.2 Molecules 83

The first step it to find a suitable starting vector for the iteration, \vec{X}_0 . This is done as described below. The correction $\delta \vec{X}$ giving the next improved estimate of \vec{X} is computed as follows. Assume after n iterations we have

$$\vec{X}_n + \vec{F}(\vec{X}_n) = \vec{R}_n. \tag{139}$$

Then we require that

$$\vec{X}_n + \delta \vec{X} + \vec{F}(\vec{X}_n + \delta \vec{X}) = \vec{R} \tag{140}$$

or

$$\vec{X}_n + \delta \vec{X} + \vec{F}(\vec{X}_n) + \mathcal{J} \cdot \delta \vec{X} = \vec{R}, \tag{141}$$

hence

$$(\mathcal{J}+1)\cdot\delta\vec{X}=\vec{R}-\vec{R_n}.\tag{142}$$

The elements of the Jacobian $\mathcal J$ are defined as

$$\mathcal{J}_{i,j} = \frac{\partial F_i}{\partial x_i}.\tag{143}$$

Since we know that

$$F_i(\vec{X}) = \frac{x_i}{x_e} \sum_{k=1,N} D_{i,k} x_k (1 + \delta_{i,k}) \quad \text{for } i = 1, N$$
 (144)

and

$$F_{N+1}(\vec{X}) = -\sum_{i=1,N} x_i \, \overline{Z}_i,\tag{145}$$

we can readily evaluate $\mathcal{J}_{i,j}$.

We find from Eqs.(144) and (145)

$$\mathcal{J}_{i,j} = \frac{\partial F_i}{\partial x_j} = D_{i,j} \frac{x_i}{x_e} \quad \text{for } i = 1, N \text{ and } i \neq j$$
 (146)

$$\mathcal{J}_{i,i} = \frac{\partial F_i}{\partial x_i} = \sum_{k \neq i} D_{i,k} \frac{x_k}{x_e} + 4 D_{i,i} \frac{x_i}{x_e} = \sum_{k=1,N} D_{i,k} \frac{x_k}{x_e} + 3 D_{i,i} \frac{x_i}{x_e} \quad \text{for } i = 1, N$$
 (147)

$$\mathcal{J}_{i,N+1} = \frac{\partial F_i}{\partial x_e} = -\frac{x_i}{x_e^2} \sum_{k=1,N} D_{i,k} \, x_k \, (1 + \delta_{i,k}) \quad \text{for } i = 1, N$$
 (148)

$$\mathcal{J}_{N+1,j} = \frac{\partial F_{N+1}}{\partial x_i} = -\overline{Z}_i \quad \text{for } j = 1, N$$
 (149)

$$\mathcal{J}_{N+1,N+1} = \frac{\partial F_{N+1}}{\partial x_e} = 0 \tag{150}$$

With this information, we can solve Eq.(142) for $\delta \vec{X}$, and obtain the next estimate

$$\vec{X}_{n+1} = \vec{X}_n + \delta \vec{X} \tag{151}$$

Once the iteration has converged, the molecule densities can be computed from Eq.(127).

12.2.3 Criterion for convergence

The criterion for convergence is currently:

$$|x_i^{(n+1)} - x_i^{(n)}| \le 1 \cdot 10^{-4} f_i \tag{152}$$

and

$$|x_i^{(n)} + \sum_{k} D_{i,k} \frac{x_i^{(n)} x_k^{(n)}}{x_e^{(n)}} (1 + \delta_{i,k}) - f_i| \le 1 \cdot 10^{-4} f_i$$
(153)

for all elements i. The maximum number of iterations is 15.

84 12 IONDIS

12.2.4 Initial guess

The initial concentrations of free atoms and ions of elements involved in molecule formation, x_i , are computed as follows.

First, we assume that no molecules are formed and so the initial x_i are set to f_i ,

$$x_{i,0} = f_i \tag{154}$$

for all elements. From this, the electron fraction x_e is computed as

$$x_{e,0} = \max \left\{ x_{e,\min}, \ f_e + \sum_{i \in \{i_{mol}\}} x_i \, \overline{Z}_i \right\},$$
 (155)

where $x_{e,\text{min}} = 1 \cdot 10^{-10}$. Using this value for x_e , we compute the molecule concentrations $x_{i,k}$ according to Eq.(127). If the resulting

$$x_{i,k} \le 1 \cdot 10^{-5} \min\{x_i, x_k\},\tag{156}$$

the formation of this molecule is considered negligible, and no correction of x_i , x_k and $x_{i,k}$ is necessary. If

$$1 \cdot 10^{-5} \min\{x_i, x_k\} < x_{i,k} \le \min\{x_i, x_k\}, \tag{157}$$

molecule formation is no longer negligible, but also not exhaustive. In this case, the molecule concentrations must be iterated, but the initial guesses for $x_{i,k}$, x_i and x_k need not be changed. Finally, if

$$x_{i,k} > \min\left\{x_i, x_k\right\},\tag{158}$$

then molecule formation is exhaustive, and the initial guesses for $x_{i,k}$, x_i and x_k are changed. We compute x_i and x_k as the equilibrium values that would result if only this particular molecule was present. If the molecule consists of two atoms of the same element, the condition is (see Eq.(130))

$$2D_{i,i}\frac{x_i^2}{x_a} + x_i - f_i = 0 ag{159}$$

which has the solution

$$x_{i,0} = \frac{2 f_i}{1 + \sqrt{1 + 8 f_i D_{i,i} / x_{e,0}}}.$$
 (160)

If the molecule consists of two different atoms, we have two conditions, namely (see Eq.(130))

$$D_{i,k} \frac{x_i x_k}{x_e} + x_i - f_i = 0$$

$$D_{i,k} \frac{x_i x_k}{x_e} + x_k - f_k = 0$$
(161)

From this we see that

$$x_i - x_k = f_i - f_k \equiv \Delta. \tag{162}$$

Then we have

$$D_{i,k} \frac{(x_k + \Delta) x_k}{x_e} + x_k - f_k = 0$$
 (163)

or

$$\frac{D_{i,k}}{x_e} x_k^2 + \left(1 + \Delta \frac{D_{i,k}}{x_e}\right) x_k - f_k = 0.$$
 (164)

Assuming that $f_i \ge f_k$, and hence $\Delta \ge 0$, the solution for x_k can be written as

$$x_{k,0} = \frac{2 f_k}{(1 + \Delta D_{i,k}/x_{e,0}) + \sqrt{(1 + \Delta D_{i,k}/x_{e,0})^2 + 4 f_i D_{i,k}/x_{e,0}}},$$
(165)

12.2 Molecules 85

and for x_i we simply have

$$x_{i,0} = x_{k,0} + \Delta. {166}$$

For each molecule, the values of $x_{i,0}$, $x_{k,0}$ obtained for the current molecule from Eq.(160) or Eqns.(165), (166) are compared to the previous values $x_{i,0}^{(n)}$, $x_{k,0}^{(n)}$ (obtained from the same conditions for a previous molecule). The new estimate of is then set to the minimum of previous and current estimate

$$x_{i,0}^{(n+1)} = \min \left\{ x_{i,0}, \ x_{i,0}^{(n)} \right\}$$

$$x_{k,0}^{(n+1)} = \min \left\{ x_{k,0}, \ x_{k,0}^{(n)} \right\}$$
(167)

The initial guess for the current molecule is then computed as

$$x_{i,k} = D_{i,k} \frac{x_{i,0}^{(n+1)} x_{k,0}^{(n+1)}}{x_{e,0}}.$$
(168)

For simplicity (and stability), the initial guess for the electron fraction is not updated when changing the initial guesses x_i for the elements involved in molecule formation.

12.2.5 Variable names

DAB	$D_{i,k}/x_e$	
DF00	$\vec{R} - \vec{R}_n$	
FRACEL	x_e	
FRACEL0	f_e	
FRACEL1	$\sum_{i \in \{i_{mol}\}} f$	$C_i \overline{Z}_i$
FRACI	f_i	
FRACJ	$x_i S_{i,j}$	(atoms and ions, $j = 1 \dots 4$)
	$x_{i,k}$	(molecules)
FREEI	x_i	
NATMOL	N	
PNUC	$N_{\rm Kern} k T$	$r = P_e/x_e$
RIJSUM	F_i	
SAHAJ	$S_{i,j}$	(atoms and ions, $j = 1 \dots 4$)
	$K_{i,k}$	(molecules)
ZEFF	\overline{Z}_i	

86 13 IONOPA

13 ionopa

LINFOR3D computes opacities, level populations, pressures and densities with the IDL/GDL routine ionopa.pro. It has evolved quite considerably over many versions of LINFOR3D and this routine has now been replaced by ionopa2.pro. It calls on the IONDIS library described above, is fairly easy to use, and can be used separately from LINFOR3D to compute various properties for 1D and 3D models. As this routine has developed, the call sequence has changed significantly. The call sequence described here is correct for the last version of ionopa.pro, which was running as of LINFOR3D version 5.1.5 and retired after version 6.1.1:

```
ionopa, temp, pin, alam, pout, densnc, okappa, osigma, pgas=pgas, $
    namj=namj, fracj=fracj, zeta=zeta, init=init, $
    dm=dm, dalpha=dalpha, avm=avm, ehe=ehe, abupath=abupath, $
    nami=nami, abui=abui
```

A brief description of all entries into ionopa are now listed.

description : gas temperature(s) in kelvins input/output : input required : always type : float properties : scalar, 1D array, 2D array, 3D array: must have same dimensions as pin values : 5777, [4000:6000]

13.2	pin		
	description	:	input pressure(s) in dyn/cm ²
	input/output	:	input
	required	:	always
	type	:	float
	properties	:	scalar, 1D array, 2D array, 3D array: must have same dimensions as temp
	values	:	1e4, [1e4:5e4]

13.3	alam		
	description	:	wavelength range in angstroms
	input/output	:	input
	required	:	always
	type	:	float
	properties	:	scalar, 1D array
	values	:	5500, [4000:6000]

13.4 pout

description : output pressure(s) in dyn/cm²

input/output : output required : always type : float

properties : same dimensions as temp and pin, i.e. scalar, 1D, 2D, 3D array

values : 1e4, [1e4:5e4]

13.5 densnc

description : number densities of atomic nuclei

input/output : output required : always type : float

properties : same dimensions as temp and pin, i.e. scalar, 1D, 2D, 3D array

values : 1.0e14

13.6 okappa

description : true absorption continuum opacity in cm² per nucleus

input/output : output required : always type : float

properties : [N temp, N alam] if alam is an array, otherwise [N temp]

values : 1.0e-22

13.7 osigma

description : scattering continuum opacity in cm² per nucleus

input/output : output required : always type : float

properties : [N temp, N alam] if alam is an array, otherwise [N temp]

values : 1.0e-27

Continuum opacity is given by okappa + osigma

88 13 IONOPA

13.8 pgas

description : toggles pin and pout

input/output : input
required : optional
type : switch
properties : scalar
values : 0 or 1

pgas = 0: ionopa assumes that pin is the electron pressure and pout is the gas pressure (default).

pgas = 1: ionopa assumes that pin is the gas pressure and pout is the electron pressure (usual case).

13.9 namj

description : input ion identifier

input/output : input required : always type : float

properties : scalar, 1D array

values : 2600.0, [2600.0, 2601.0, 5600.0]

13.10 fracj

description : fractional number density n_i / densnc, where n_i is the number density

of namj elements in ionization stage j

input/output : output required : optional type : float

properties : [N temp, N namj] if namj is an array, otherwise [N temp]

values : 3.30554e-12

13.11 zeta

description : number densities such that $zeta = fracj / U_j(T)$

input/output : output required : optional type : float

properties : [N temp, N namj] if namj is an array, otherwise [N temp]

values : 4.53707e-10

13.12 init

description : type of abu file

input/output : input

required : for initialisation only

type : integer properties : scalar values : 1, 2, 3

init = 1: abu file is defined as kiel.abu

init = 2: abu file is defined as cifist2006.abu

init = 3: abu file is defined as special.abu

13.13 dm

description : gas metallicity

input/output : input

required : for initialisation only

type : float properties : scalar values : -1.0, 0.0

13.14 dalpha

description : gas alpha enhancement, $[\alpha/Fe]$

input/output : input

required : for initialisation only

type : float properties : scalar values : 0.0, 0.4

Affects elements O, Ne, Mg, Si, S, Ar, Ca and Ti

13.15 avm

description : average mass of nucleus for chemical composition defined by init

input/output : output required : optional type : float properties : scalar

values : 2.08985e-24

90 13 IONOPA

13.16 ehe

description : ratio of helium to hydrogen number densities

input/output : output
required : optional
type : float
properties : scalar
values : 0.0851139

13.17 abupath

description : path to directory where abu file defined by init can be found

input/output : input required : always type : string properties : scalar

values : getenv('LINFOR3D_ABU')

13.18 nami

description : ion identifier from abu file defined by init

input/output : output required : optional type : integer properties : 1D array

values : 100, 200, 300, ..., 9200

13.19 abui

description : corresponding abundances of ions in nami

input/output : output required : optional type : float properties : 1D array

values : 12.0000, 10.9300, 1.10000, ..., -0.470000

13.20 Example

In order to use ionopa it first needs to be initialised. The initialisation tells ionopa properties of the model such as its metallicity, chemical abundances, alpha enhancement. An example of the initialisation may look as follows:

```
IDL> ionopa, 0.0, 0.0, 0.0, pout, densnc, okappa, osigma, init = 2, $
IDL> dm = -1.0, dalpha = 0.4, abupath = getenv('LINFOR3D_ABU'), $
IDL> nami = nami, abui = abui, ehe = ehe, avm = avm0
```

13.20 Example 91

% Compiled module: IONOPA.

Not all of those options are required, however. Once initialised, ionopa can be executed. The input parameters should be used instead of the 0.0 values used to initialise.

```
IDL> ionopa, Tin, Pin, alam, pele, densnc, okappa, osigma, /pgas, $
IDL> namj = ions, fracj = fracj, zeta = zeta
```

92 14 IONOPA2

14 ionopa2

ionopa2 replaced ionopa in LINFOR3D version 6.2.0 onwards. The inputs and outputs of ionopa2 are fairly similar to ionopa, but there are certain differences:

```
ionopa2, temp, qin, alam, pe, pg, densnc, okappa, osigma, qflg=qflg, $
    namj=namj, fracj=fracj, zeta=zeta, init=init, $
    dm=dm, dalpha=dalpha, avm=avm, ehe=ehe, abupath=abupath, $
    nami=nami, abui=abui
```

A brief description of all entries into ionopa2 are now listed.

description : gas temperature(s) in kelvins input/output : input required : always type : float properties : scalar, 1D array, 2D array, 3D array: must have same dimensions as qin values : 5777, [4000:6000]

14.2	qin		
	description	:	input quantities in cgs units
	input/output	:	input
	required	:	always
	type	:	float
	properties	:	scalar, 1D array, 2D array, 3D array: must have same dimensions as temp
	values	:	1e4, [1e4:5e4]

14.3	alam		
	description	:	wavelength range in angstroms
	input/output	:	input
	required	:	always
	type	:	float
	properties	:	scalar, 1D array
	values	:	5500, [4000:6000]

```
description : electron pressure(s) in dyn/cm<sup>2</sup>
input/output : output
required : always
type : float
properties : same dimensions as temp and qin, i.e. scalar, 1D, 2D, 3D array
values : 1e4, [1e4:5e4]
```

14.5 pg

description : gas pressure(s) in dyn/cm²

input/output : output required : always type : float

properties : same dimensions as temp and qin, i.e. scalar, 1D, 2D, 3D array

values : 1e4, [1e4:5e4]

14.6 densnc

description : number densities of atomic nuclei

input/output : output required : always type : float

properties : same dimensions as temp and qin, i.e. scalar, 1D, 2D, 3D array

values : 1.0e14

14.7 okappa

description : true absorption continuum opacity in cm² per nucleus

input/output : output required : always type : float

properties : [N temp, N alam] if alam is an array, otherwise [N temp]

values : 1.0e-22

14.8 osigma

description : scattering continuum opacity in cm² per nucleus

input/output : output required : always type : float

properties : [N temp, N alam] if alam is an array, otherwise [N temp]

values : 1.0e-27

Continuum opacity is given by okappa + osigma

94 14 IONOPA2

14.9 qflg

description : toggles qin input/output : input

required : optional. Set to 0 if ignored

type : switch
properties : scalar
values : 0, 1, 2, 3

qflg = 0: qin is defined as the electron pressure, P_e (default).

qflg = 1: qin is defined as the gas pressure (usual case), $P_{\rm gas}$.

qflg = 2: qin is defined as $P_{gas} - P_e$.

qflg = 3: qin is defined as continuum opacity per unit volume, densnc * (okappa + osigma).

14.10 namj

description : input ion identifier

input/output : input required : always type : float

properties : scalar, 1D array

values : 2600.0, [2600.0, 2601.0, 5600.0]

14.11 fracj

description : fractional number density n_i / densnc, where n_i is the number density

of namj elements in ionization stage j

input/output : output required : optional type : float

properties : [N temp, N namj] if namj is an array, otherwise [N temp]

values : 3.30554e-12

14.12 zeta

description : number densities such that $zeta = fracj / U_i(T)$

input/output : output required : optional type : float

properties : [N temp, N namj] if namj is an array, otherwise [N temp]

values : 4.53707e-10

14.13 init

description : type of abu file

input/output : input

required : on initalisation or when more than one abu file has been initialised

type : integer properties : scalar

values : -3, -2, -1, 1, 2, 3

init = 1: abu file is defined as kiel.abu

init = 2: abu file is defined as cifist2006.abu

init = 3: abu file is defined as special.abu

init = -1: initialise composition 1 from memory*.

init = -2: initialise composition 2 from memory*.

init = -3: initialise composition 3 from memory*.

*Used if ionopa2 has been initialised for more than one abu file.

14.14 dm

description : gas metallicity

input/output : input

required : for initialisation only

type : float properties : scalar values : -1.0, 0.0

14.15 dalpha

description : gas alpha enhancement, $[\alpha/Fe]$

input/output : input

required : for initialisation only

type : float properties : scalar values : 0.0, 0.4

Affects elements O, Ne, Mg, Si, S, Ar, Ca and Ti

96 14 IONOPA2

14.16 avm

description : average mass of nucleus for chemical composition defined by init

input/output : output required : optional type : float properties : scalar

values : 2.08985e-24

14.17 ehe

description : ratio of helium to hydrogen number densities

input/output : output
required : optional
type : float
properties : scalar
values : 0.0851139

14.18 abupath

description : path to directory where abu file defined by init can be found

input/output : input required : always type : string properties : scalar

values : getenv('LINFOR3D_ABU')

14.19 nami

description : ion identifier from abu file defined by init

input/output : output required : optional type : integer properties : 1D array

values : 100, 200, 300, ..., 9200

14.20 abui

description : corresponding abundances of ions in nami

input/output : output required : optional type : float properties : 1D array

values : 12.0000, 10.9300, 1.10000, ..., -0.470000

14.21 Example 97

14.21 Example

Like ionopa, ionopa2 must first be initialised.

```
IDL> ionopa2, 0.0, 0.0, 0.0, pele, pgas, densnc, okappa, osigma, $
IDL> init = 2, dm = 0.0, dalpha = 0.0, avm=avm, ehe=ehe, $
IDL> abupath=getenv('LINFOR3D_ABU'), nami=nami, abui=abui
% Compiled module: IONOPA2.
```

Now that ionopa2 has been initialised, it can be executed.

```
IDL> ionopa2, tin, qin, alam, pele, pgas, densnc, okappa, osigma, $
IDL> qflg = 1, namj = ions, fracj = fracj, zeta = zeta
```

Additionally, ionopa2 can be initialised more than once for more than one abu file.

```
IDL> %----- initialise 1 -----
IDL> ionopa2, 0.0, 0.0, 0.0, pele, pgas, densnc, okappa, osigma, $
IDL> init = 2, dm = 0.0, dalpha = 0.0, avm = avm2, ehe = ehe2, $
IDL> abupath = getenv('LINFOR3D_ABU'), nami = nami2, abui = abui2
% Compiled module: IONOPA2.

IDL> %----- initialise 2 -----
IDL> ionopa2, 0.0, 0.0, 0.0, pele, pgas, densnc, okappa, osigma, $
IDL> init = 3, dm = 0.0, dalpha = 0.0, avm = avm3, ehe = ehe3, $
IDL> abupath = getenv('LINFOR3D_ABU'), nami = nami3, abui = abui3
```

Once it has been initialised for the requested parameters it can be executed without being reinitialised.

```
IDL> %---- execute 1 ----
IDL> ionopa2, tin2, qin2, alam, pele2, pgas2, densnc2, okappa2, osigma2, $
IDL> qflg = 1, namj=[ions], fracj = fracj2, zeta = zeta2, init = -2
IDL> %---- execute 2 ----
IDL> ionopa2, tin3, qin3, alam, pele3, pgas3, densnc3, okappa3, osigma3, $
IDL> qflg = 1, namj=[ions], fracj = fracj3, zeta = zeta3, init = -3
```

Note the use of init in these instances. As ionopa2 has been initialised for more than one abu file, init should be included from its memory.

Index

α -elements, 29, 89, 95	Change log, 9
Contribution functions, 13	Main program
Continuum flux, 13	run_flag, 23
Continuum Intensity, 13	Calling sequence, 19
Equivalent width, 15	
Line depression, 14	Parameter input
Line flux, 14	execution flags, 23
Line Intensity, 14	linfor_setcmd, 23
plotting, 73	Plotting
Curve-of-Growth	contribution functions, 73
CMD, 36, 39, 40	Curve-of-Growth, 74
computations, 39	synthesis, 72
CONST, 64	Redictive transfer 10
plotting, 74	Radiative transfer, 10
RESULT, 71	Structures, 20
CDI	ABU, 62
GDL	ATOM, 62
cmake, 75	CMD, 62
Eigan3, 75	CONST, 62
installing GDL, 75	CONTF, 65
Linfor3D in parallel, 76	CONTF3D, 71
Linfor3D with GDL, 75	IMUPHI, 67
plotting, 72	INFO, 64
Grey test case, 15	LINE, 64
IDL, 20	MAPS, 68
plotting, 72	RESULT, 69
IONDIS	flow field, 20
atomic information, 79	ray system, 20
ionopa, 86	spectrum, 20
ionopa2, 92	
treatment of molecules, 80	Transfer equation
	the continuum intensity, 10
Line Data	the line depression, 12
ABO van der Waals broadening, 55	the line intensity, 11
blends, 52	UIO
data format: -1, 43	definition, 8
data format: 0, 44	library, 20
data format: 1, 45	UIO information, 60
data format: 2, 47	uio_restore, 60
data format: 3, 48	uio_save, 57
data format: 4, 49	uiosave, 23, 57, 59, 62, 65, 68, 71, 72
data format: 5, 50	diosave, 23, 37, 39, 62, 63, 66, 71, 72
data format: 6, 50	
data format: 7, 51	
Natural broadening, 56	
Quadratic stark broadening, 53	
Van der Waals broadening, 54 line.dat, 43	
LINFOR3D, 7	
LIM OKJU, I	